



High-Efficiency Full Bridge Buck-Boost DC/DC Controller

General Description

The VP3402 is a high efficiency full-bridge buck-boost DC/DC controller designed for use in voltage step-up or step-down converting application. It operates over a wide input range from 4.2V to 30V and is capable of adjusting output voltage up to 30V. Current mode control scheme also makes it wide bandwidth and good transient response. The operating frequency can be adjusted simply with an external resistor or any external clock source between 100kHz and 600kHz. Its internal gate driver provides 2A peak current driving capability.

The VP3402 also provides input/output average current sensing and limiting function, optional CCM/DCM operation, optional EMI improvement and power status indication pin. This device features lots of protection such as cycle-by-cycle current limiting, input under-voltage lockout, output over voltage, short, over-temperature and optional hiccup mode in sustained overload conditions. Programmable soft-start circuitry reduces the inrush current at start-up.

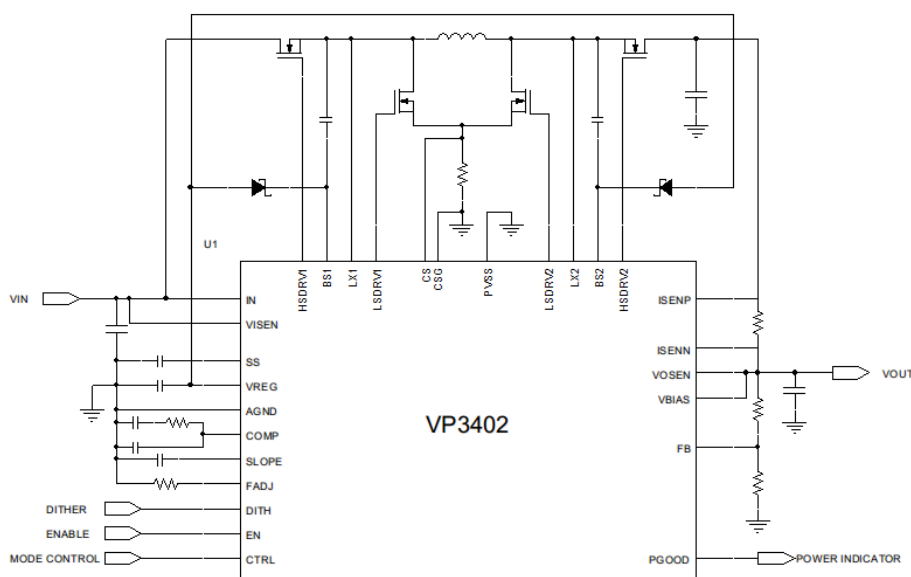
Features

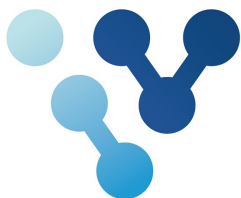
- 4-Switch Step-Up/Step-Down Operation
- Wide Input Voltage from 4.2V to 30V
- Adjustable Output Voltage from 0.8V to 30V
- Adjustable 100kHz~600kHz Clock Frequency
- Optional Frequency Synchronization/Dithering
- 2A Peak Current Limit Using Internal Driver
- Current Mode Operation
- External RC Compensation
- Programmable Soft-Start and Input UVLO
- High Efficiency at Light Loads
- Power Good Indication
- Output Over-Voltage Protection
- Output Short Voltage Protection
- Current Limit and Over Temperature Protection
- TQFN4x5-28 Green Package with RoHS Compliant

Applications

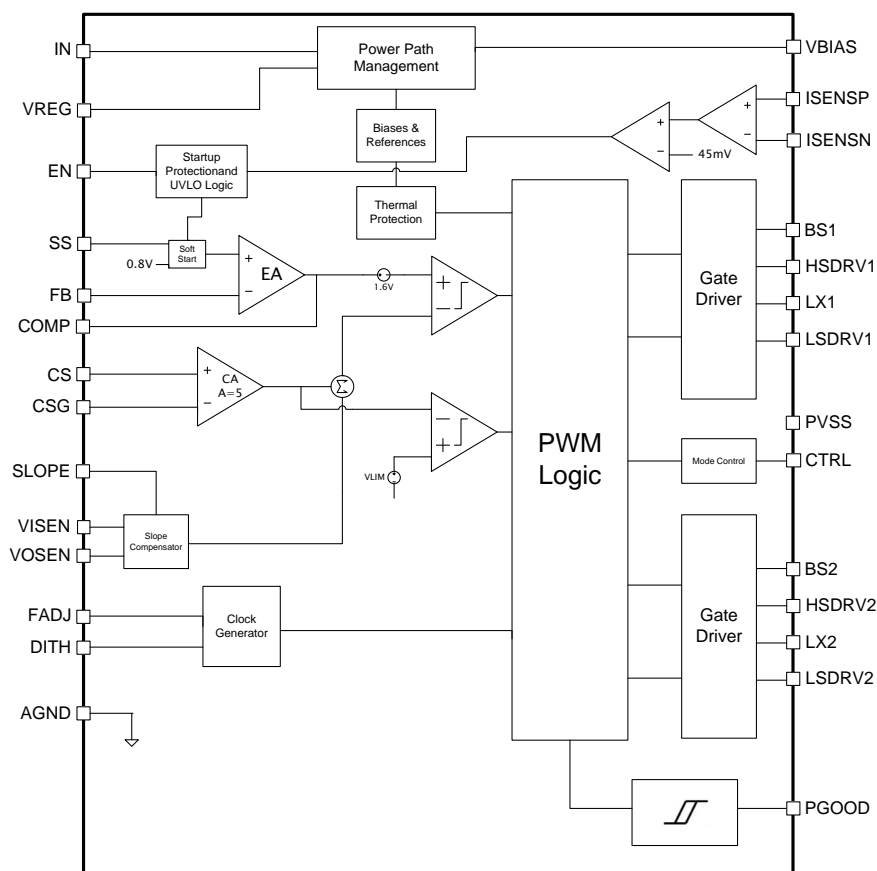
- USB Power Delivery
- Industrial Power Supplies
- Battery and Super-Capacitor Charging
- LED Lighting

Typical Application

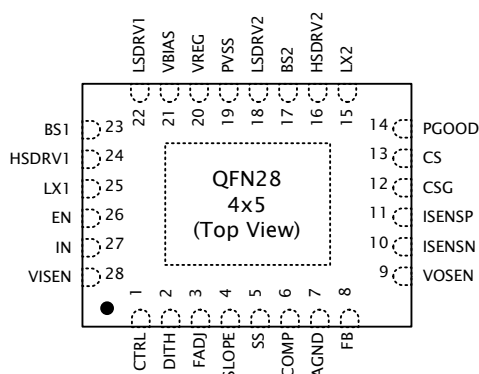


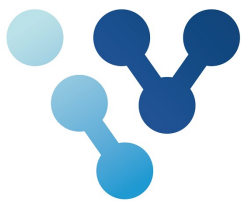


Functional Block Diagram



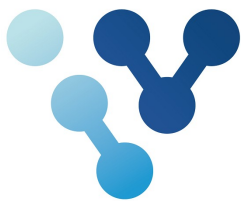
Pin Assignments





Pin Descriptions

No.	Pin	I/O/P	Function Description
1	CTRL	I	Mode Control. Connect a resistor to ground to configure CCM/DCM operation and hiccup mode. See functional description for setting table.
2	DITH	I	Frequency Dithering Adjust. Connect a capacitor to ground to make the VP3402 PWM modulation frequency swing in $\pm 5\%$ of the frequency specified by FADJ external resistor. Leave this pin unconnected for disabling this feature.
3	FADJ	I	Frequency Adjust or Synchronization. A resistor connected from this pin to ground simply sets the oscillator frequency. An external clock signal at this pin will synchronize the controller.
4	SLOPE	I	Slope Compensation. Connect a capacitor to ground to perform slope compensation for buck-boost operating stabilization.
5	SS	I	Soft-Start Programming. Connect a capacitor to ground to program the soft-start time.
6	COMP	O	Compensation. Use a Type II RC//C network to do proper loop compensation.
7	AGND	P	Analog Ground.
8	FB	I	Output Feedback. Connect the external resistor divider network from output to this pin to sense output voltage.
9	VOSEN	I	Output Voltage Sense Input. Connect this pin close to output capacitors.
10	ISENSN	I	Average Current Limit Negative Input.
11	ISENSP	I	Average Current Limit Positive Input.
12	CSG	I	Negative Current Amplifier Input.
13	CS	I	Positive Current Amplifier Input.
14	PGOOD	OD	Power Good Indicator (Open Drain). PGOOD is pulled low if FB pin is outside $\pm 10\% V_{FB}$ regulation.
15	LX2	I	2nd Switching Node. LX2 is the 2nd switching node.
16	HSDRV2	O	2nd High-Side Drive Pin.
17	BS2	P	Bootstrap I/O for 2nd High-Side Switch.
18	LSDRV2	O	2nd Low-Side Drive Pin.
19	PVSS	P	Power Ground. The ground connection to all low-side gate drivers.
20	VREG	O	Internal Regulator. Connect a capacitor to ground.
21	VBIAS	I	Output Bias Connection. Connect this pin to output to improve efficiency.
22	LSDRV1	O	1st Low-Side Drive Pin.
23	BS1	P	Bootstrap I/O for 1st High-Side Switch.
24	HSDRV1	O	1st High-Side Drive Pin.
25	LX1	I	1st Switching Node. LX1 is the 1st switching node.
26	EN	I	Chip Enable. For $EN < 0.7V$, the VP3402 enters shutdown mode. For $0.7V < EN < 1.23V$, VREG is enabled but no PWM switching. For $EN > 1.3V$, PWM switching is enabled. TTL Logic levels with compliance to V_{IN} .
27	IN	P	Power Supply Input. Connect this pin to power supply.
28	VISEN	I	Input Voltage Sense Input. Connect this pin close to input capacitors.
-	Exposed Pad	P	Thermal Ground. The pad should be soldered to the analog ground with low thermal resistance.



Absolutely Maximum Ratings

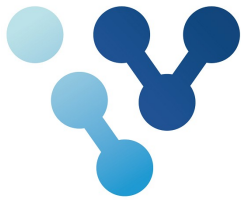
Over operating free-air temperature range, unless otherwise specified (* 1)

Symbol	Parameter	Limit	Unit
V_{IN}	Supply voltage range	-0.3 to 42	V
$V_{IN(HV)}$ (EN/ VISEN/ VOSEN/ ISENSP/ ISENSN)	High voltage input range	-0.3 to 40	V
$V_{IN(HV)}(VBIAS)$	High voltage bias input range	-0.3 to 40	V
$V_{IN(LV)}$ (COMP/ FB/ SS/ DITH/ FADJ/ SLOPE)	Low voltage input range	-0.3 to 3.6	V
V_{REG} (VREG/ CTRL/ PGOOD)	Internal regulator related pin input	-0.3 to 5.5	V
LSDRV1, LSDRV2 BS1, HSDRV1 to LX1 BS2, HSDRV2 to LX2	Input voltage range	-0.3 to 5.5	V
$V_{SW}(LX1 / LX2)$	Switch node voltage	-1 to 42	V
$V_{BS}(BS1, BS2)$	Bootstrap node voltage	-0.3 to 5.5	V
CS, CSG	Sense pins differential input voltage range	-0.3 to 0.3	V
$T_{J(MAX)}$	Operating junction temperature range	150	°C
T_{STG}	Storage temperature range	-65 to 150	°C
Electrostatic discharge	Human body model	2	kV
Electrostatic discharge	Machine model	200	V
θ_{JC}	Thermal resistance (Junction to Case)	27	°C/W
θ_{JA}	Thermal resistance (Junction to Air)	50	°C/W

(*1): Stress beyond those listed at "absolute maximum rating" table may cause permanent damage to the device. These are stress rating ONLY. For functional operation are strongly recommend follow up "recommended operation conditions" table.

Recommended Operating Conditions

Symbol	Parameter	Specification		Unit
		Min	Max	
$V_{IN(IN)}$	Supply voltage	4.2	30	V
$V_{IN(VISEN)}$	Supply Input with VBIAS connected (VBIAS \geq 5V or IN \geq 4.5V)	2.5	30	V
VBIAS	Auxiliary supply voltage	6	30	V
$V_{IN(VOSEN)}$	Output sense input voltage range	0.8	30	V
EN	Enable pin input voltage	0	30	V
ISENSP, ISENSN	Sense pin input voltage	0	30	V
f_{OSC}	Switching voltage range	100	600	kHz
T_A	Operating free-air temperature range	-40	85	°C
T_J	Operating temperature range	-40	125	°C

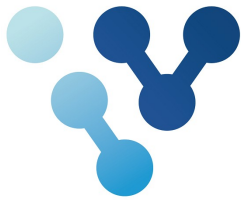


Electrical Characteristics

Operating condition $V_{IN}=24V$, $T_J=25^{\circ}C$, $R_T=82k$, unless otherwise specified (* 1)

Symbol	Parameter	Test Condition	Specification			Unit
			Min	Typ.	Max	
SUPPLY VOLTAGE						
I _{SD}	Shutdown mode supply current	V _{EN} =0V		12	16	μA
I _{STBY}	Standby mode supply current	V _{EN} =1.1V, non-switching		0.6	2	mA
I _Q	Operating current	V _{EN} =2V, V _{FB} =0.7V		1.65	4	mA
ENABLE/UVLO						
V _{EN(STBY)}	Standby threshold voltage	V _{EN} rising	0.55	0.79	0.97	V
I _{EN(STBY)}	Standby mode pin source current	V _{EN} =1.1V		2	3	μA
V _{EN(OPER)}	Operating threshold voltage	V _{EN} rising	1.17	1.23	1.29	V
I _{HYS(OPER)}	Operating hysteresis current	V _{EN} =2.4V	1.5	3.5	5.5	μA
VBIAS						
V _{VBIAS(SW)}	Internal bias switchover voltage			6		V
ERROR AMPLIFIER						
V _{FB}	Feedback reference voltage	V _{EN} =2V, FB connect to COMP	0.788	0.8	0.812	V
I _{FB}	Feedback bias current	V _{FB} =0.1V			0.1	μA
BW	Unity gain bandwidth			2		MHz
I _{COMP}	COMP source current	FB=V _{REF} -300mV, COMP=0V		280		μA
	COMP sink current	FB=V _{REF} +300mV, COMP=3V		280		
g _{M(EA)}	Error amplifier trans-conductance			1270		μΩ
VREG						
V _{REG}	Internal regulation voltage	EN=2V, VBIAS pin open, VREG pin open	5.1	5.3	5.5	V
V _{UV}	VREG UVLO threshold	V _{REG} rising		3.3		V
R _{OUT(VREG)}	LDO Output impedance	I _{OUT} =0.03A, V _{IN} =3.5V		9.3	16	Ω
	UVLO hystersis			160		mV
I _{OUT(VREG)}	VREG maximum supply current	V _{IN} =3.5V, V _{REG} =0V		65		mA
PGOOD						
V _{PGOOD}	PGOOD trip ratio for FB (Falling)	Ratio to V _{FB}		-9		%
	PGOOD trip ratio for FB (Rising)	Ratio to V _{FB}		10		%
	Hystersis			1.6		%
I _{LEAK(PGOOD)}	PGOOD leakage current	FB=0.8V, V _{PGOOD} =5V			100	nA
I _{SINK(PGOOD)}	PGOOD sink current	FB=0V, V _{PGOOD} =0.4V	2	4.2	6.5	mA

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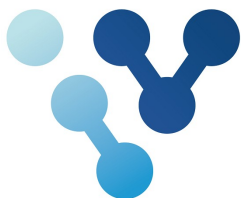


Electrical Characteristics (cont.)

Operating condition $V_{IN}=24V$, $T_J=25^{\circ}C$, $R_T=82k$, unless otherwise specified (* 1)

Symbol	Parameter	Test Condition		Specification			Unit
				Min	Typ.	Max	
FREQUENCY/SYNC/DITHER							
PW _{SYNC}	SYNC input pulse width			75		500	ns
f _{sw}	PWM switching frequency	V _{FB} =0.7V	R _T =133kΩ		200		kHz
			R _T =47kΩ		500		kHz
V _{SYNCH}	SYNC input high threshold			2.1			V
V _{SYNCL}	SYNC input low threshold					1.2	V
V _{DITHER}	Dither high threshold				1.27		V
	Dither low threshold				1.16		V
I _{DITHER}	Dither source/sink current	DITHER=1.1V, DITHER=1.3V			10.5		μA
SOFT START							
I _{SS}	Soft start pull-up current	V _{SS} =0V		4.30	5.65	7.25	μA
V _{SS(CL)}	Soft start clamp voltage	SS open			1.27		V
ΔV _{FB} -V _{SS}	FB to SS offset voltage	V _{SS} =0V			-15		mV
GATE DRIVER							
I _{HSDRV1,2}	Gate driver peak source current	V _{BS1} -V _{LX1} =5.3V			1.8		A
	Gate driver peak sink current	V _{BS1} -V _{LX1} =5.3V			2.2		
I _{LSDRV1,2}	Gate driver peak source current	V _{BS2} -V _{LX2} =5.3V			1.8		
	Gate driver peak sink current	V _{BS2} -V _{LX2} =5.3V			2.2		
R _{HSDRV1,2}	Gate driver pull-up resistance	V _{BS1,2} -V _{LX1,2} =5.3V			1.9		Ω
	Gate driver pull-down resistance	V _{BS1,2} -V _{LX1,2} =5.3V			1.3		
R _{LSDRV1,2}	Gate driver pull-up resistance	I _{LSDRV1,2} =0.1A			2		Ω
	Gate driver pull-down resistance	I _{LSDRV1,2} =0.1A			1.5		
V _{UV(BS1,2)}	BS1,2 to LX1,2 UVLO threshold	HSDRV1,2 shut off			2.73		V
	BS1,2 to LX1,2 UVLO hystersis	HSDRV1,2 begin switching			280		mV
	BS1,2 to LX1,2 threshold for re-fresh pulse				4.45		V
t _{DTH}	HSDRV1,2 off to LSDRV1,2 on dead time				45		ns
t _{DTL}	LSDRV1,2 off to HSDRV1,2 on dead time				45		ns
OUTPUT OVP							
V _{OVP}	Output overvoltage threshold	Relative to FB			0.86		V
	Output overvoltage hystersis				21		mV

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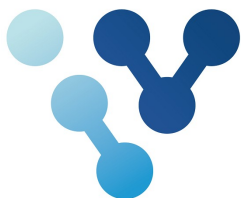


Electrical Characteristics (cont.)

Operating condition $V_{IN}=24V$, $T_J=25^{\circ}C$, $R_T=82k$, unless otherwise specified (* 1)

Symbol	Parameter	Test Condition	Specification			Unit
			Min	Typ.	Max	
CURRENT LIMIT						
V _{CS(BUCK)}	Buck mode current limit threshold (Valley)	V _{IN} =V _{VISNS} =24V, V _{VOSNS} =12V, V _{SLOPE} =0V	53.2	76	98	mV
V _{CS(BOST)}	Boost mode current limit threshold (Peak)	V _{IN} =V _{VISNS} =12V, V _{VOSNS} =18V, V _{SLOPE} =0V	119	170	221	
I _{BIAS(CS/CSG)}	CS/CSG pin bias current	V _{CS} =V _{CSG} =V _{SLOPE} =0V		-75		μA
I _{OFFSET(CS/CSG)}	CSG pin offset current	V _{CS} =V _{CSG} =V _{SLOPE} =0V			14	
CONSTANT CURRENT LOOP						
V _{SNS}	Average current loop regulation	V _{ISNSN} =24V, sweep I _{SNSP} , Measure V _{SS}	43	50	57	mV
I _{SNS}	ISNSN/ISNSP pin bias currents	V _{IN} =V _{ISNSP} =V _{ISNSN} =24V		7		μA
g _{M(CS)}	Current sense amplifier trans-conductance	V _{ISNSP} -V _{ISNSN} =55mV, V _{SS} =0.5V		1		mΩ
SLOPE COMPENSATION						
I _{SLOPE}	Buck adaptive slope current	V _{IN} =V _{VISNS} =24V, V _{VOSNS} =12V, V _{SLOPE} =0V	24	30	35	μA
	Boost adaptive slope current	V _{IN} =V _{VISNS} =12V, V _{VOSNS} =18V, V _{SLOPE} =0V	13	17	21	
g _{M(SLOPE)}	Slope compensation amplifier trans-conductance			2		μΩ
MODE						
I _{MODE}	Source current out of MODE pin	MODE=0V	17	20	23	μA
V _{DCM_HIC}	DCM with hiccup threshold voltage		0.6	0.7	0.76	V
V _{CCM_HIC}	CCM with hiccup threshold voltage		1.18	1.28	1.38	
V _{CCM}	CCM no hiccup threshold voltage		2.22	2.4	2.6	
THERMAL PROTECTION						
T _{SHUTDOWN}	Thermal shutdown trip point			160		°C
	Thermal shutdown hystersis			15		

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Functional Descriptions

The VP3402 is a high efficiency full bridge buck-boost controller with wide input voltage range. In addition to buck mode and boost mode, VP3402 also operates in buck-boost mode with excellent efficiency and low ripple output voltage when V_{IN} close to V_{OUT} .

VP3402 integrates two half-bridge N-channel MOSFET gate drivers and is designed to work with 4 external MOSFET switches. When V_{IN} is greater than V_{OUT} , the VP3402 PWM control works in valley current mode. The inductor current should be monitored for cycle-by-cycle current limit and is sensed through an external sense resistor connected to the source of low-side MOSFET switches and power ground.

When V_{IN} is lower than V_{OUT} , the VP3402 PWM control works in peak current mode. For the application cases of lower V_{IN} (e.g. below than 6V) and higher V_{OUT} , VP3402 is capable of supporting bias VBIAS terminal with V_{OUT} . In this condition, internal regulator source would be switched from V_{IN} to V_{OUT} for higher gate driver bias so that better switching efficiency would be achieved.

Besides cycle-by-cycle current limiting, the VP3402 supports average current sense scheme for either input or output current detection. Soft-start is also supported with an external capacitor connected to ground to eliminate inrush current and voltage overshoot during startup.

VP3402 supports continuous conduction mode (CCM) for noise sensitive application such as audio or radio frequency use and discontinuous conduction mode (DCM) for higher light load efficiency such as backup power application. For the output overload/short condition VP3402 provides optional hiccup mode to reduce the heat and damage during sustained overload case. If the hiccup mode

is disabled the controller remains in a cycle-by-cycle current limit until the overload case is fixed. Use CTRL terminal to configure CCM/DCM operation and hiccup mode selection.

The VP3402 supports over-voltage protection and power good status indication. If the output feedback voltage exceeds then 7.5% or above nominal reference V_{REF} (0.8V) the high side drivers would be turn off. PGOOD terminal would be externally pulled high when FB pin voltage is regulated within +10% and -9% centered with V_{REF} .

The VP3402 can operate in shutdown state, standby state and normal operation state. It can be configured with setting EN terminal with 3 distinct voltage ranges.

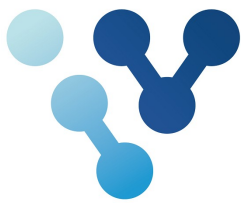
Operation States and UVLO

The VP3402 has chip enable and under-voltage lock out protection. When EN pin voltage is below than standby threshold 0.7V, the controller enters the shutdown state and most of the functional blocks are disabled including V_{REG} regulator.

When EN voltage is greater than standby threshold but less than the operating threshold 1.23V, both internal V_{REG} regulator and VBIAS bias input are enabled but the controller will still not start up and hence no switching.

When EN voltage is greater than operating threshold, the controller will start switching if the V_{REG} is also above V_{REG} under-voltage threshold (3.3V). If V_{REG} is still under UV threshold, the VP3402 will not switch. Table 1 shows the relation between the state and EN pin threshold voltage range.

To implement UVLO protection, the simplest way is to use a resistor network from V_{IN} to AGND with



Functional Descriptions (cont.)

the mid-point connect to EN pin. The turn-on threshold can be obtained by equation 1.

$$(1) \quad V_{IN(UVLO)} = 1.23V \times \left(1 + \frac{R_{EN2}}{R_{EN1}}\right) - R_{EN2} \times 1.5\mu A$$

$$(2) \quad \Delta V_{HYS(UVLO)} = 3.5\mu A \times R_{EN2}$$

Equation 2 shows the hysteresis between the UVLO turn-on and turn-off threshold and can be obtained with this equation. Beware of the EN pin source current is $3.5\mu A$ when EN pin voltage is above $1.23V$.

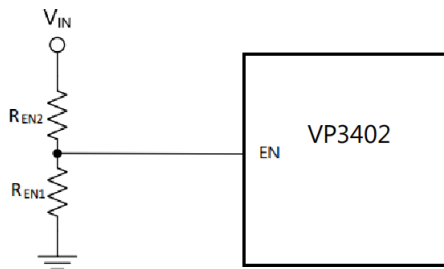


Figure 1. Programming EN pin

EN	V _{REG}	State
EN < 0.7V	N/A	Shutdown
0.7V < EN < 1.23V	N/A	Standby
EN > 1.23V	V _{REG} < 3.3V	Standby
EN > 1.23V	V _{REG} > 3.3V	Operating, Switching

Table 1. EN pin threshold voltage

Frequency Adjustment

It is simply to use an external resistor to adjust the PWM clock frequency. Connect a resistor from FADJ terminal to AGND to program switching frequency from 100kHz to 600kHz. Equation 3 shows how to calculate the external resistor:

$$(3) \quad R_T = \frac{\left(\frac{1}{f_{sw}} - 200ns\right)}{37pF}$$

The VP3402 can be synchronized with external clock source. Figure 2 demonstrates the connec-

tion to AC clock source. The external clock frequency should be higher than resistor programmed frequency. Beware of the pulse width of the external PWM clock should be in range from 75ns to 500ns and the pulse amplitude must not exceed 3.3V.

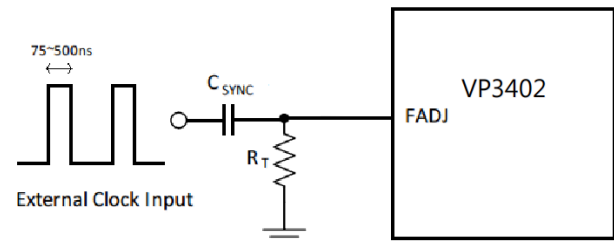


Figure 2. External Clock Synchronization

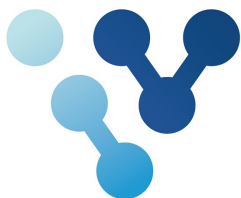
Frequency dithering is an important skill to improve EMI performance. Connect a capacitor from DITH pin to AGND to enable this function. Equation 4 shows the calculation of dithering capacitance:

$$(4) \quad C_{DITH} = \frac{10\mu A}{f_{sw} \times 0.24V}$$

Connect the DITH pin to ground to disable this function. Dithering function is also disabled when using external clock input.

Soft Start

The VP3402 provides soft start scheme to prevent transient during startup and could be adjusted by a soft start capacitor connected from SS terminal to AGND. During powering up, an internal current source charges the soft start capacitor with $5\mu A$. When the SS pin voltage below the feedback reference V_{REF} , soft-start block raises the FB voltage with the same slope as the SS pin. After SS pin voltage exceeds V_{REF} , the soft-start period is finished and the output voltage is almost reached to desired output value. Soft-start time is calculated



Functional Descriptions (cont.)

by equation 5:

$$(5) \quad t_{ss} = \frac{C_{ss} \times 0.8V}{5\mu A}$$

SS pin will be discharged in the following 3 conditions, EN falling below UVLO voltage and VREG UV threshold, enter hiccup mode and thermal shutdown state. When average current limiting is active, the SS pin would be also discharged by the constant current loop trans-conductance amplifier to limit the current.

Average Current Limit

To implement current limit protection of input or output, a constant current trans-conductance amplifier is integrated in the VP3402. An additional current sense resistor connected in series with the ISENSP and ISENSN pins to monitor the voltage drop and compare it with internal 50mV reference. If the voltage drop is greater than 50mV then the constant current loop trans-conductance amplifier gradually discharges the soft-start capacitor to pull low the output voltage to limit the input or output current. Use equation 6 to obtain the current limit value. Short ISENSP and ISENSN to disable this function.

$$(6) \quad I_{CL(AVG)} = \frac{50mV}{R_{SENS}}$$

CCM/DCM Operation

CTRL pin	Mode	Protection
Direct to VREG	CCM	Cycle-by-cycle limit
Use 91k to AGND	CCM	Hiccup
Use 47k to AGND	DCM+CCM	Hiccup
Direct to AGND	DCM+CCM	Cycle-by-cycle limit

Table 2. CTRL Pin Selections

The VP3402 allows the operation mode change of continuous conduction (CCM) or discontinue con-

duction (DCM). For noise sensitive application such as audio amplifier, the switching noise needs to be filtered to prevent any hearable noise. CCM operation the inductor current can flow in either direction and the controller switches at a fixed frequency regardless of the load current.

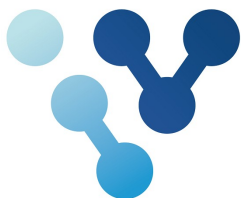
In DCM operation, when the inductor current reaches zero the synchronous rectifier MOSFETs emulate diodes as LSDRV1 or HSDRV2 turn-off for the rest of the PWM cycle at light load to reduce switching losses as possible. DCM operation results in reduced and variable frequency operation which increases light load efficiency of the converter.

Table 2 shows how the CTRL pin configures the operation mode. The mode is latched at startup.

Over-current Protection

In buck operation, the sensed valley voltage across R_{SENSE} is limited to 76mV. If the sensed value is not below this threshold during the buck switch off-time, the high-side buck switch skips a cycle. In boost operation, the maximum peak voltage across the R_{SENSE} is limited to 170mV. If the peak current in boost switch causes the CS pin to exceed this threshold, the low-side boost switch is turned-off for the rest of the clock.

Use proper connection networks defined in Table 2 to configure VP3402 in the appropriate working manner. If the hiccup mode (CCM or DCM) is enabled, the controller shuts down after detecting cycle-by-cycle current for 128 cycles and then the soft-start capacitor is discharged. After 4000 clock cycles the SS pin resumes to charge soft-start capacitor again and the controller starts over again. If the hiccup mode is not enabled, the VP3402 will perform cycle-by-cycle current limit when over-



Functional Descriptions (cont.)

load condition occurs.

Output Over-voltage Protection

VP3402 will turn off the 2 gate drivers when the feedback voltage is 7.5% greater than the nominal reference voltage V_{REF} . Once the feedback value falls in 5% of V_{REF} , the VP3402 resumes switching.

Internal Regulator and VBIAS Input

Since the VP3402 uses half-bridge gate drivers and high side NMOSFET gate bias should be generated from internal V_{REG} with boot-strap circuits. For V_{IN} is less than the certain of value, the V_{REG} voltage tracks V_{IN} with few voltage drop. Otherwise the internal regulator V_{REG} voltage will be fixed and regulated. The on/off scheme follows the control mechanism of EN pin as previous described.

When V_{OUT} is greater than V_{REG} nominal value plus one more diode drop, the internal regulator will use V_{OUT} to regulate internal V_{REG} instead of using V_{IN} . In buck mode, connect VBIAS pin to V_{OUT} with V_{OUT} value greater than 7V will improve the efficiency. Please be aware that the voltage on VBIAS pin should not exceed then 36V.

If V_{IN} is lower and working topology is boost, use higher output voltage and feed it back to V_{OUT} to generate internal V_{REG} is a good idea. For this case, place a series blocking diode between the input power source and IN terminal to prevent V_{REG} back-feeding into IN pin through internal MOSFET body diode.

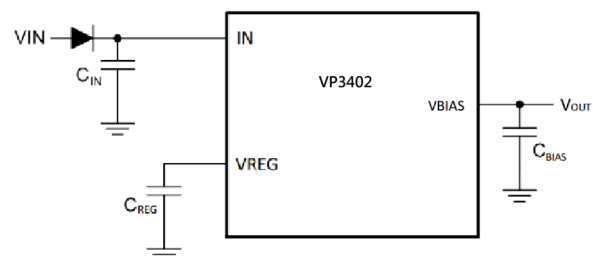


Figure 3. VREG and VBIAS

V_{REG} grounding capacitor is good to use a 1 μ F ceramic capacitor and is better to be placed close to VREG pin.

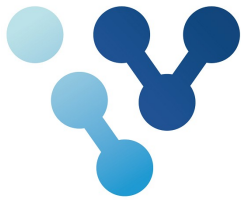
Power Good Indicator

PGOOD terminal is pulled high when the voltage at the FB pin is within range of -9%~+10% of the nominal V_{REF} voltage. Otherwise the PGOOD is pulled low. Since the PGOOD is open drain output, it is needed to add pull-up resistor and the pull down strength of the internal MOSFET is about 4.2mA. Since the MOSFET is low voltage device, do not connect the pull-up resistor to 5.5V or higher.

Slope Compensation

The VP3402 performs a slope compensation based on the current sense signal monitored across the CS and CSG pins with the composition of the V_{IN} , V_{OUT} and SLOPE pin signals. The result is compared to the COMP error voltage by PWM modulator.

The current mode controllers require slope com-



Functional Descriptions (cont.)

compensation for stable current loop operation. In peak current mode the duty is 50% or above and below 50% in valley current mode. Use a capacitor to connect between SLOPE pin and AGND to fine tune optimal slope for various V_{IN} and V_{OUT} combination.

Loop Compensation

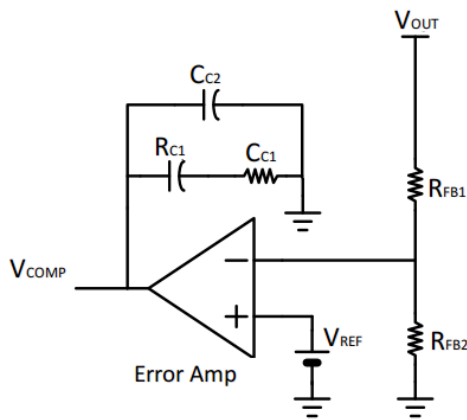


Figure 4. Error Amplifier Compensation Network

Figure 4 shows the internal loop compensation structure. The trans-conductance amplifier output range is from 0.3V to 3V. The COMP pin output range will limit the possible V_{IN} and output current. Type II PI compensation is formed with R_{C1} - C_{C1} to AGND in parallel with another pole compensator C_{C2} .

The VP3402 will operate in buck, boost and buck-boost mode and the compensation is separated into two considerations. In buck mode, the bottom value of COMP dominates the maximum possible V_{IN} for which the controller can regulate output voltage at no load. Equation 7 shows how to calculate V_{COMP} as function of V_{IN} at no load in CCM operating.

(7)

$$V_{COMP(BUCK)} = 1.6V - A_{CS} \cdot R_{SENSE} \cdot \frac{V_{OUT}}{2 \cdot L_1 \cdot F_{SW}} \cdot (1 - D_{BUCK}) - \frac{2\mu S \cdot (V_{IN} - V_{OUT}) + 6\mu A}{C_{SLOPE} \cdot F_{SW}} \cdot (1 - D_{BUCK})$$

Where D_{BUCK} is given by equation 8.

$$D_{BUCK} = \frac{V_{OUT}}{V_{IN}} \quad (8)$$

To increase the maximum V_{IN} range of buck operation, try to change appropriate frequency, larger inductor, higher C_{SLOPE} , smaller sense resistor.

In boost mode, the minimum possible V_{IN} for which the converter can regulate the output at full load is the top value of V_{COMP} . Equation 9 shows how to calculate V_{COMP} as function of V_{IN} at full load in CCM operating.

(9)

$$V_{COMP(BOOST)} = 1.6V + A_{CS} \cdot R_{SENSE} \cdot \left(I_{OUT} \cdot \frac{V_{OUT}}{V_{IN}} + \frac{V_{IN}}{2 \cdot L_1 \cdot F_{SW}} \cdot D_{BOOST} \right) + \frac{2\mu S \cdot (V_{OUT} - V_{IN}) + 5\mu A}{C_{SLOPE} \cdot F_{SW}} \cdot D_{BOOST}$$

Where D_{BUCK} is given by equation 10.

$$D_{BOOST} = 1 - \frac{V_{IN}}{V_{OUT}} \quad (10)$$

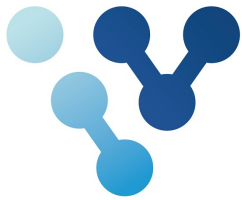
From equation 9, a larger L_1 , higher C_{SLOPE} , smaller R_{SENSE} and higher frequency could enlarge the V_{IN} range of boost operation.

Gate Drivers

The VP3402 is a full bridge controller and it contains 4 NMOSFET gate drivers. The buck half bridge drive pins are HSDRV1 and LSDRV1 as well as the boost half bridge drive pins are HSDRV2 and LSDRV2. Each gate driver is capable of sinking 2A and sourcing 1.5A peak current.

In DCM operation, LSDRV1 and HSDRV2 turn off when the inductor current reaches to zero in buck operation and HSDRV2 turns off when inductor current drops to zero in boost operation. The driver HSDRV2 would not switch unless soft-start progress is finished to prevent possible reverse current from a pre-biased output.

The low side gate drivers LSDRV1 and LSDRV2 are



biased from V_{REG} and the high side gate drivers HSDRV1 and HSDRV2 are driven from boot-strap capacitors. The boot capacitors are charged and boosted through external schottky diodes connected to VREG terminal. Avoids to use the diodes with greater forward conduction voltage V_F because the high-side gate drives bias will be greatly reduced below than 5V.

Thermal Protection

The thermal protection circuit monitors the junction temperature and turns off the VP3402 when junction temperature exceeds temperature trip point. When the protection occurs, the soft-start capacitor will be discharged and the gate drivers shut down immediately. The controller will resume switching after soft-start progress when the junction temperature is below then the thermal shut-down hysteresis value.



Application Information

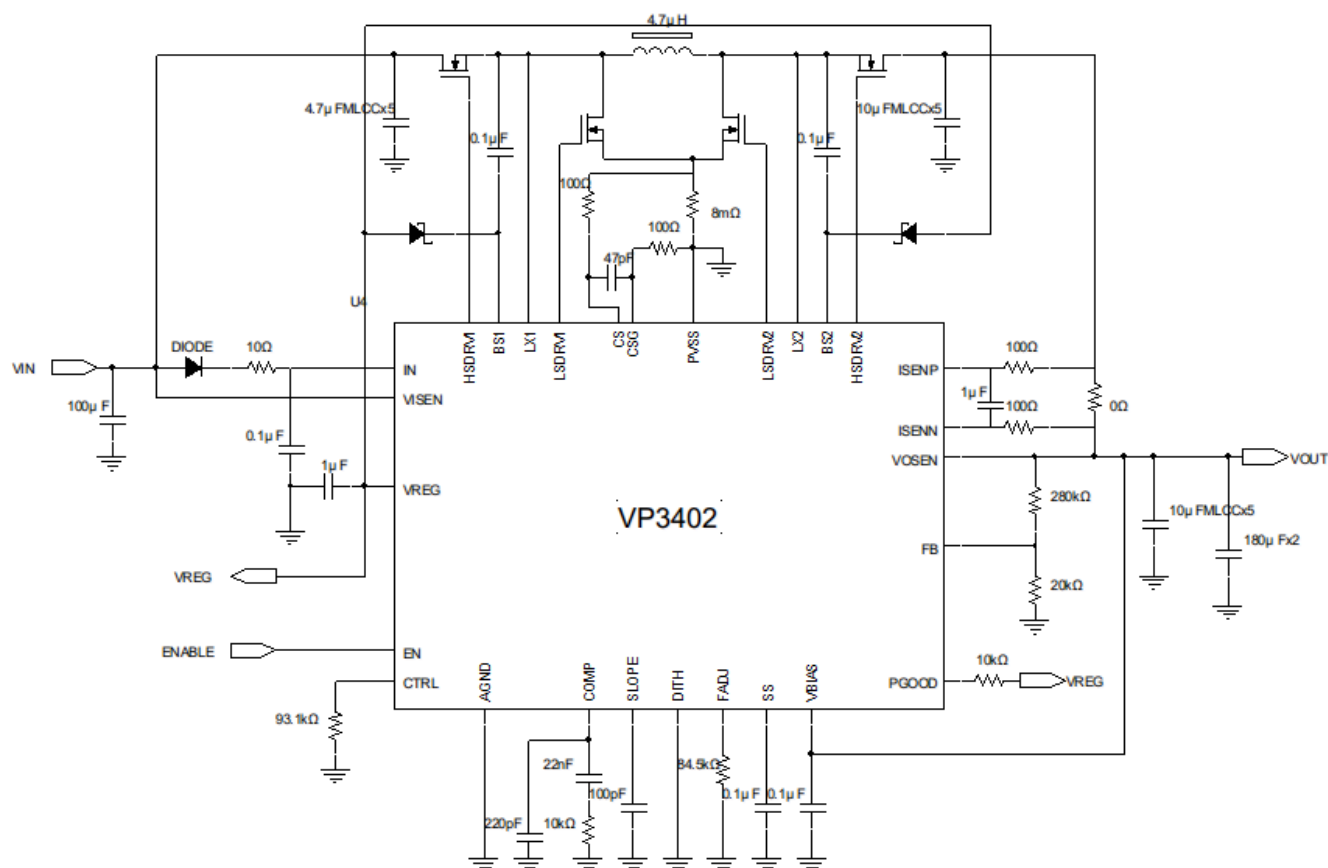
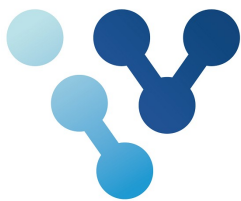


Figure 5. VP3402 Typical Application

Specification Item	Rating
Input Voltage Range	6V~30V
Output	12V
Load Current	6A maximum
Switching Frequency	300kHz
Operating Mode	CCM with Hiccup

Table 3. VP3402 Typical Application Specification



Typical Characteristics

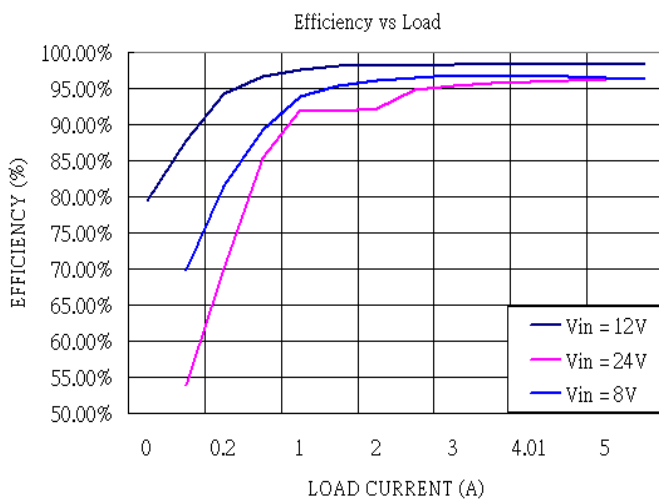
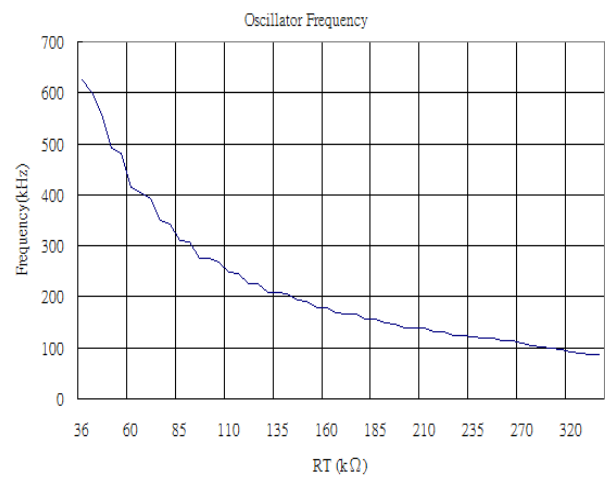
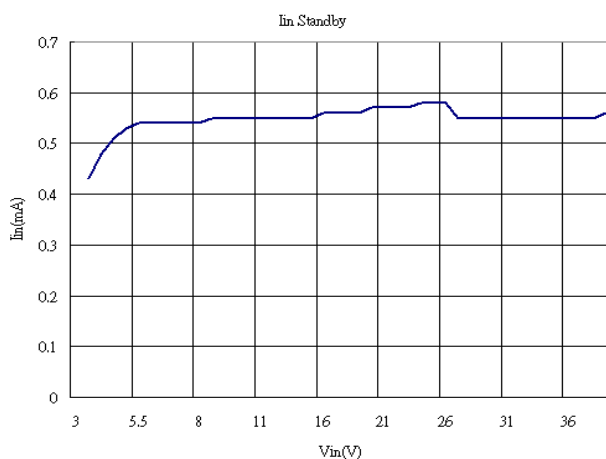
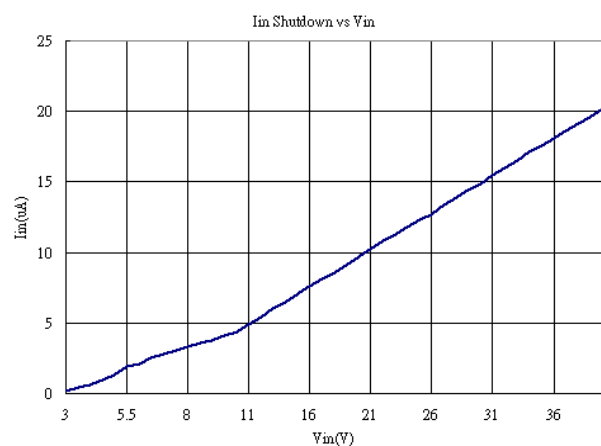
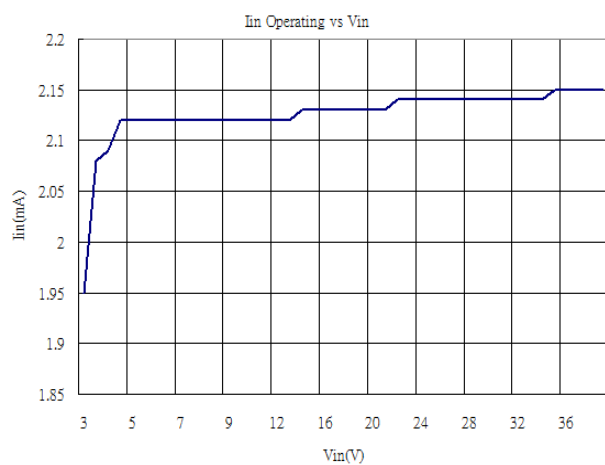
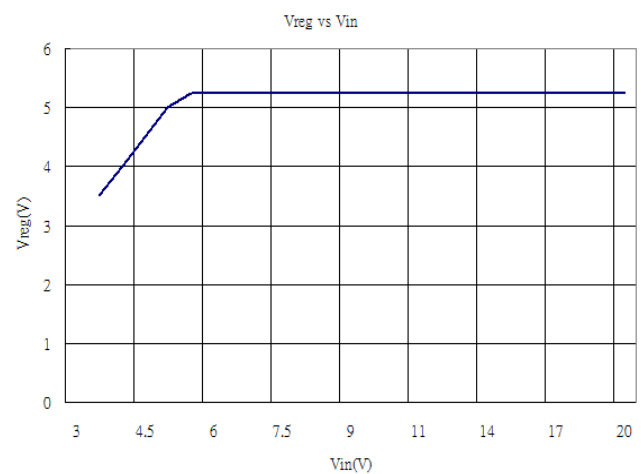
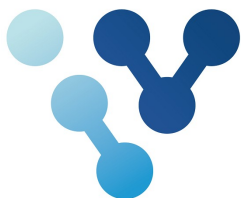


Figure 6. Efficiency

Figure 7. Frequency vs. R_T Figure 8. Standby Current vs. V_{in} Figure 9. Shutdown Current vs. V_{in} Figure 10. Operating Current vs. V_{in} Figure 11. V_{REG} value vs. V_{in}



Typical Characteristics (cont.)

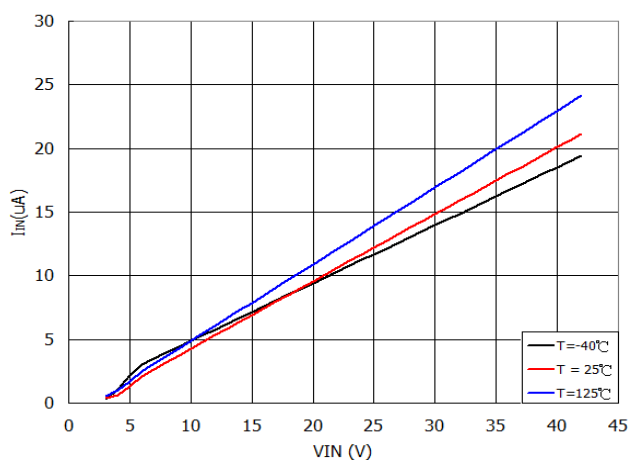


Figure 12. I_{IN} Shutdown vs. V_{IN}

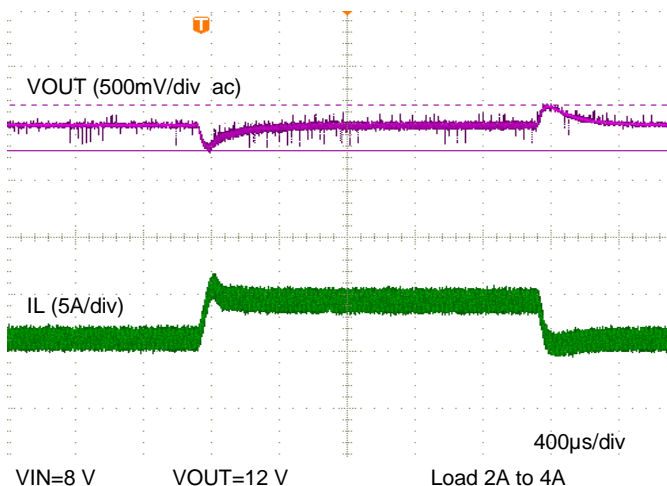


Figure 15. Load Step (Boost)

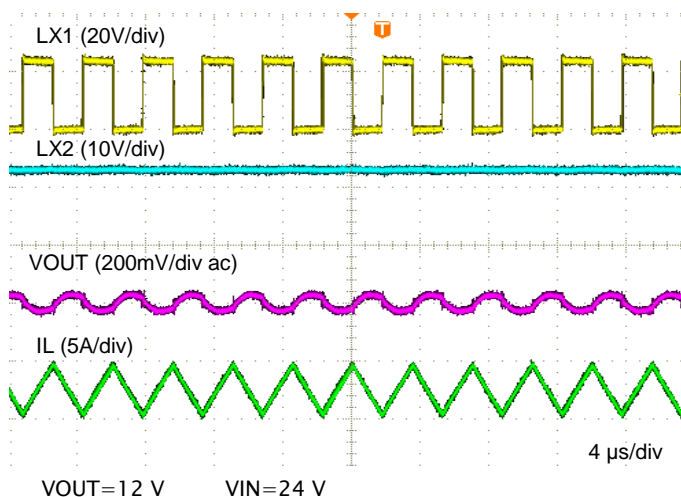


Figure 13. Forced CCM Operation (Buck)

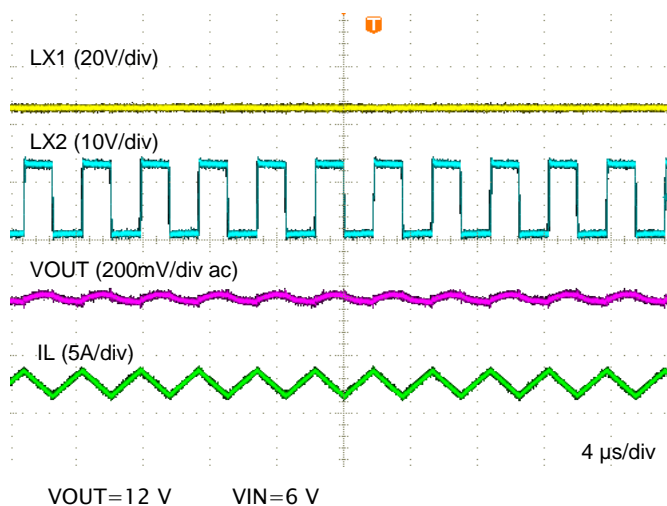


Figure 16. Forced CCM Operation (Boost)

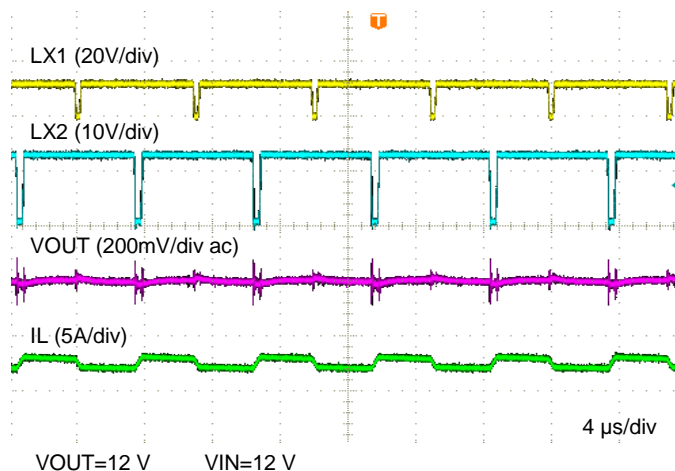


Figure 14. Forced CCM Operation (Buck-Boost)

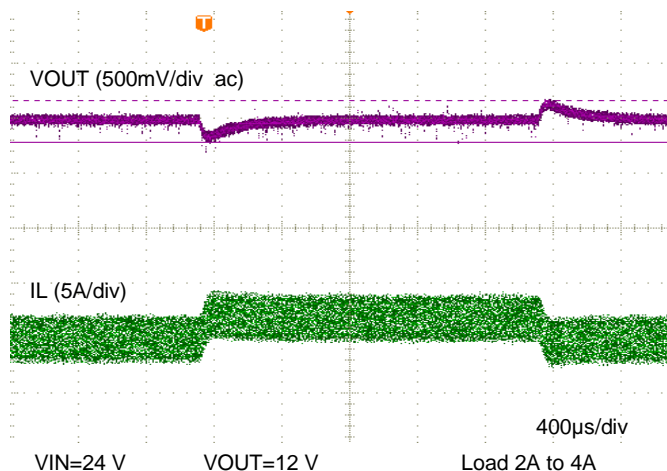
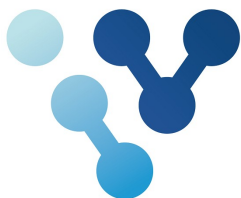


Figure 17. Load Step (Buck)



Typical Characteristics (cont.)

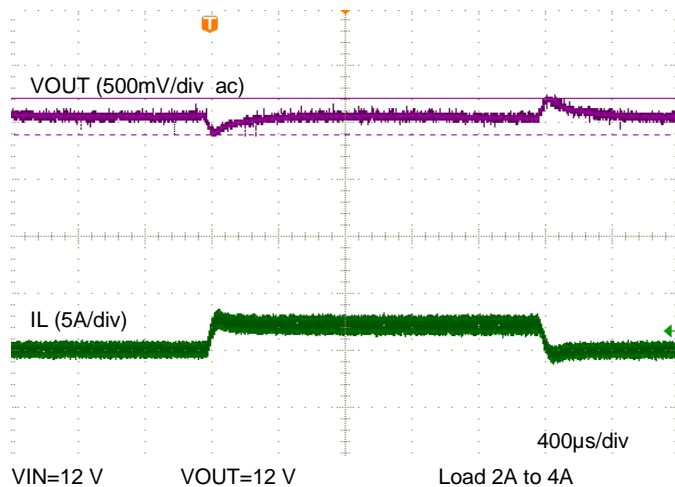


Figure 18. Load Step (Buck-Boost)

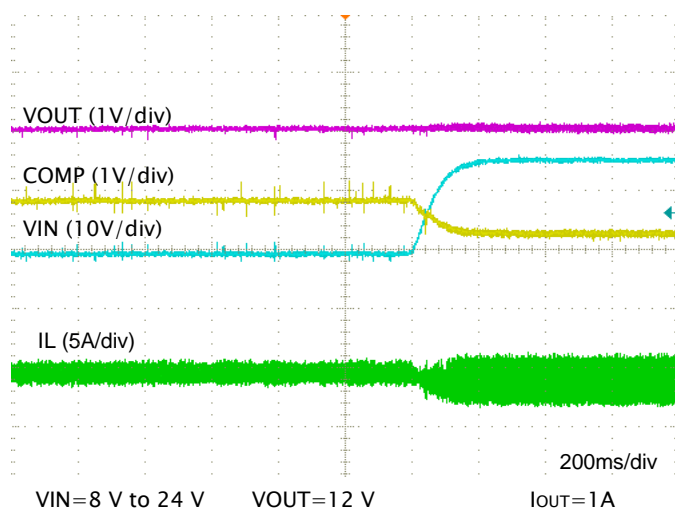


Figure 19. Line Transient

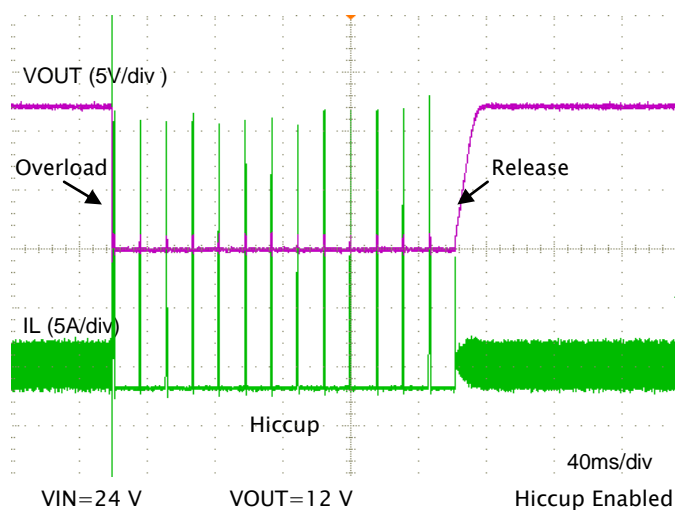
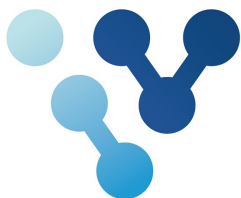
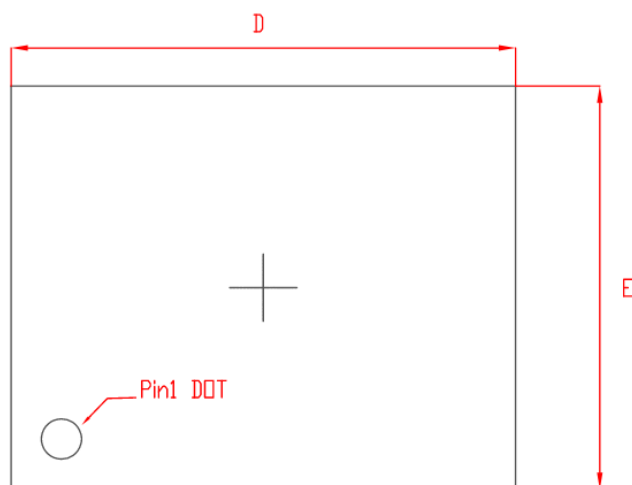


Figure 20. Hiccup Mode Current Limit

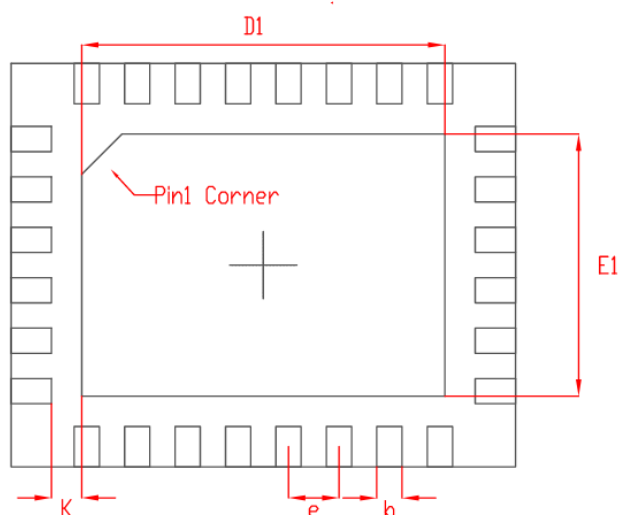


Package Information (cont.)

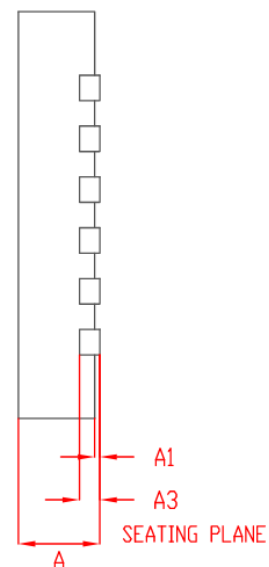
TQFN4x5-28



TOP VIEW



BOTTOM VIEW

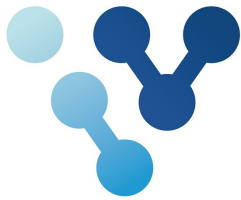


SIDE VIEW

SYMBOL	QFN4x5x0.75-28					
	MILLIMETERS			INCHES		
	MIN.	NOM.	MAX.	MIN.	NOM.	MAX.
A	0.70	----	0.80	0.028	----	0.031
A1	0.00	----	0.05	0.000	----	0.002
A3	0.203 REF			0.008 REF		
b	0.20	0.25	0.30	0.008	0.010	0.012
D	5.00 BSC			0.197 BSC		
E	4.00 BSC			0.157 BSC		
e	0.50 BSC			0.020 BSC		
D1	3.50	3.65	3.80	0.138	0.144	0.150
E1	2.50	2.65	2.80	0.098	0.104	0.110
L	0.30	0.40	0.50	0.012	0.016	0.020
K	0.20	-----	-----	0.008	-----	-----

Notes

- 1.EXPOSED PADDLE SIZE DOES NOT INCLUDE MOLD FLASH
- 2.LEAD COPLANARITY SHALL BE 0.1 MILLIMETER MAX.



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