

2A, 1MHz, 5.5V CMCOT Synchronous Step-Down Converter

The HT8097A is a high efficiency synchronous step-down DC/DC converter. Its input voltage range is from 2.7V to 5.5V and provides an adjustable regulated output voltage from 0.6V to 3.3V while delivering up to 2A of output current. The internal synchronous low on-resistance power switches increase efficiency and eliminate the need for an external Schottky diode. The Current Mode Constant-On-time (CMCOT) operation with internal compensation allows the transient response to be optimized over a wide range of loads and output capacitors.

Features

- Efficiency Up to 95%
- $R_{DS(on)}$ 110m Ω HS / 80m Ω LS
- V_{IN} Range 2.7V to 5.5V
- V_{REF} 0.6V with $\pm 2\%$ Accuracy at 25°C
- CMCOT™ Control Loop Design for Best Transient Response, Robust Loop Stability with Low-ESR (MLCC) C_{OUT}
- Soft-Start 1.2ms; PGOOD Function in SOT-23-6
- Power Saving in Light Load

Applications

- STB, Cable Modem, & xDSL Platforms
- LCD TV Power Supply & Metering Platforms
- General Purpose Point of Load (POL)

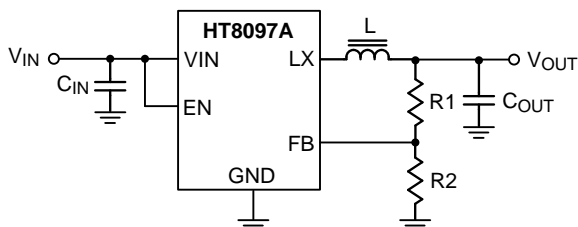
ORDERING INFORMATION



SOT23-5 T SUFFIX
HT8097ARTZ

$T_A = -40^\circ$ to 85°C for all packages.

Simplified Application Circuit

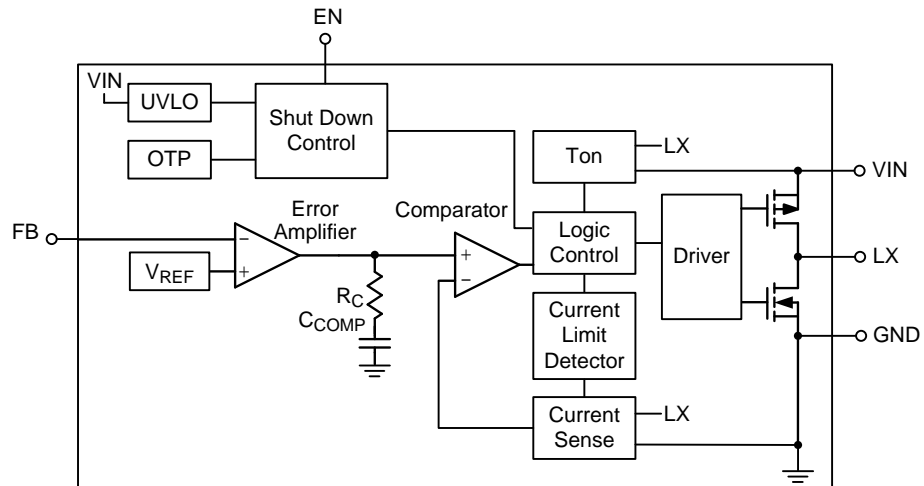


Functional Pin Description

Pin No.		Pin Name	Pin Function
SOT-23-5	SOT-23-6		
1	1	EN	Enable Control Input.
2	2	GND	Power Ground.
3	3	LX	Switch Node.
4	4	VIN	Supply Voltage Input. The HT8097A operates from a 2.7V to 5.5V input.
5	6	FB	Feedback Voltage Input. An external resistor divider from the output to GND, tapped to the FB pin, sets the output voltage.
--	5	NC	No Connect.

Function Block Diagram

For SOT-23-6 Package



Operation

The HT8097A is a synchronous low voltage step-down converter that can support the input voltage range from 2.7V to 5.5V and the output current can be up to 2A. The HT8097A uses a constant on-time, current mode architecture. In normal operation, the high side P-MOSFET is turned on when the switch controller is set by the comparator and is turned off when the Ton comparator resets the switch controller. Low side MOSFET peak current is measured by internal RSENSE. The error amplifier EA adjusts COMP voltage by comparing the feedback signal (V_{FB}) from the output voltage with the internal 0.6V reference. When the load current increases, it causes a drop in the feedback voltage relative to the reference, then the COMP voltage rises to allow higher inductor current to match the load current.

PGOOD Comparator

When the feedback voltage (V_{FB}) is higher than threshold voltage 0.54V, the PGOOD open drain output will be high impedance. The internal PG MOSFET is typical 10 Ω . The PGOOD signal delay time from EN is about 2ms.

Enable Comparator

A logic-high enables the converter; a logic-low forces the IC into shutdown mode. There is an internal pull down 1M Ω resistor at EN pin.

Soft-Start (SS)

An internal current source charges an internal capacitor to build the soft-start ramp voltage. The V_{FB} voltage will track the internal ramp voltage during soft-start interval. The typical soft-start time is 1.2ms.

Over Current Protection (OCP)

The HT8097A provides over current protection by detecting low side MOSFET valley inductor current. If the sensed valley inductor current is over the current limit threshold (3.2A typ.), the OCP will be triggered. When OCP is tripped, the HT8097A will keep the over current threshold level then cause the UV protection.

Thermal Shutdown (OTP)

The device implements an internal thermal shutdown function when the junction temperature exceeds 150°C. The thermal shutdown forces the device to stop switching when the junction temperature exceeds the thermal shutdown threshold. Once the die temperature decreases below the hysteresis of 20°C, the device reinstates the power up sequence.

Absolute Maximum Ratings (Note 1)

- Supply Input Voltage ----- -0.3V to 6.5V
- Power Dissipation, P_D @ $T_A = 25^\circ\text{C}$
 SOT-23-6 ----- 0.5W
- Package Thermal Resistance (Note 2)
 SOT-23-6, θ_{JA} ----- 197.4°C/W
- Lead Temperature (Soldering, 10 sec.) ----- 260°C
- Junction Temperature ----- -40°C to 150°C
- Storage Temperature Range ----- -65°C to 150°C
- ESD Susceptibility (Note 3)
 HBM (Human Body Model) ----- 2kV

Recommended Operating Conditions (Note 4)

- Supply Input Voltage ----- 2.7V to 5.5V
- Ambient Temperature Range ----- -40°C to 85°C
- Junction Temperature Range ----- -40°C to 125°C

Electrical Characteristics

($V_{IN} = 3.6\text{V}$, $T_A = 25^\circ\text{C}$, unless otherwise specified)

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit
Input Voltage		V_{IN}		2.7	--	5.5	V
Feedback Reference Voltage		V_{REF}		0.588	0.6	0.612	V
Feedback Leakage Current		I_{FB}	$V_{FB} = 3.3\text{V}$	--	--	1	μA
DC Bias Current			Active, $V_{FB} = 0.63\text{V}$, Not Switching	--	22	--	μA
			Shutdown	--	--	1	
Switching Leakage Current				--	--	1	μA
Switching Frequency				--	1	--	MHz
Switch On Resistance, Low		R_{NMOS}	$I_{SW} = 0.3\text{A}$	--	80	--	$\text{m}\Omega$
Switch On Resistance, High		R_{PMOS}	$I_{SW} = 0.3\text{A}$	--	110	--	$\text{m}\Omega$
Valley Current Limit		I_{LIM}		--	3.2	--	A
Under-Voltage Lockout Threshold		V_{UVLO}	VDD Rising	--	2.25	2.5	V
			VDD Falling	--	2	--	V
Over-Temperature Threshold				--	150	--	$^\circ\text{C}$
Enable Input Voltage	Logic-High	V_{IH}		1.5	--	--	V
	Logic-Low	V_{IL}		--	--	0.4	

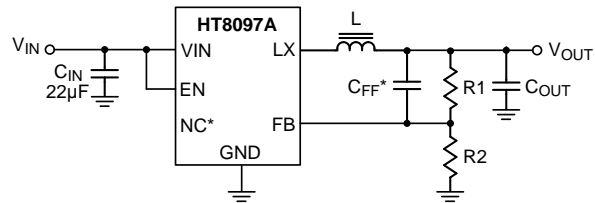
Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit
PG Pin Threshold (relative to V_{OUT})		Rising	--	90	--	%
		Falling	--	85	--	
PG Open-Drain Impedance (PG = low)			--	--	100	Ω
Soft-Start Time	T _{SS}		--	1.2	--	ms
Minimum Off Time			--	120	--	ns
Output Discharge Switch On Resistance			--	1.8	--	k Ω

Note 1. Stresses beyond those listed "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

Note 2. θ_{JA} is measured at $T_A = 25^\circ\text{C}$ on a high effective thermal conductivity four-layer test board per JEDEC 51-7.

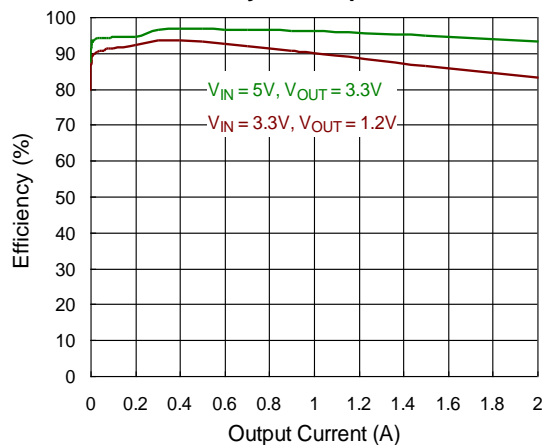
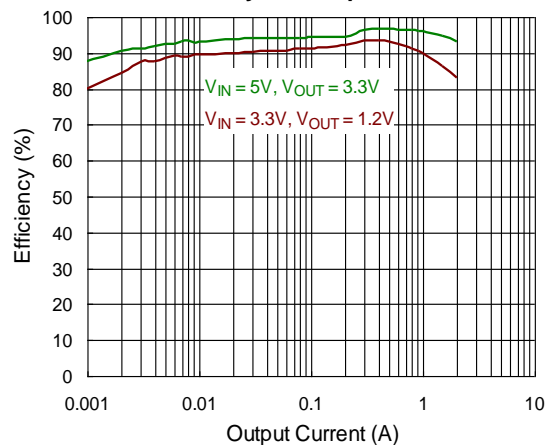
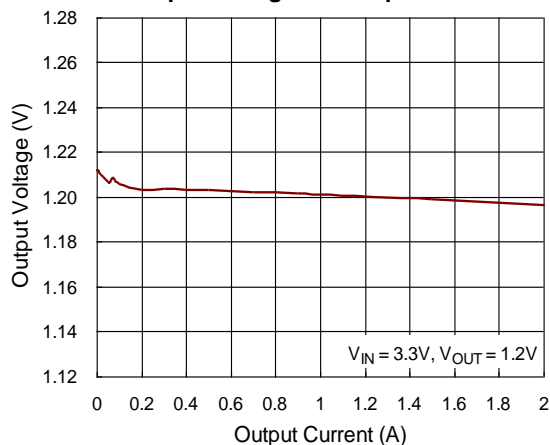
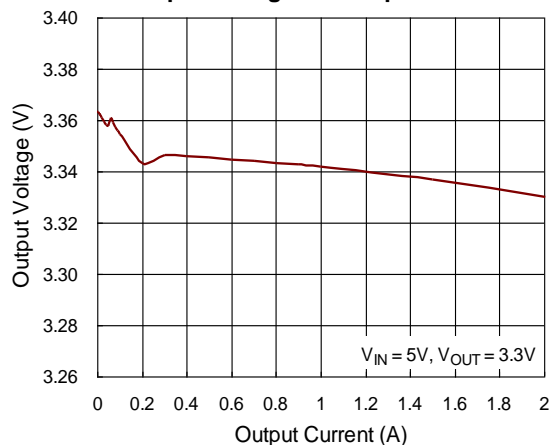
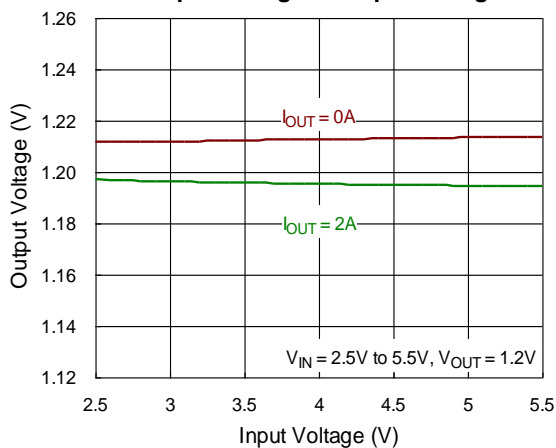
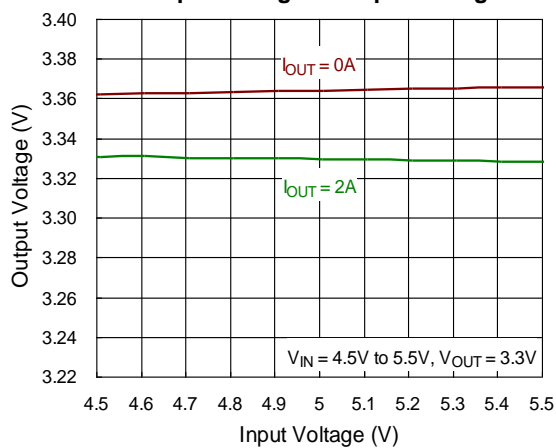
Note 3. Devices are ESD sensitive. Handling precaution recommended.

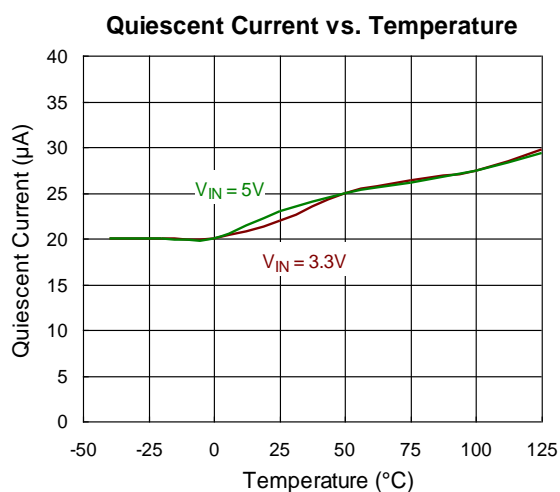
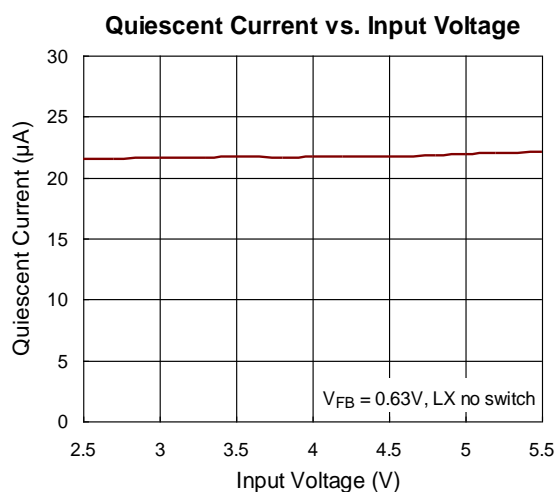
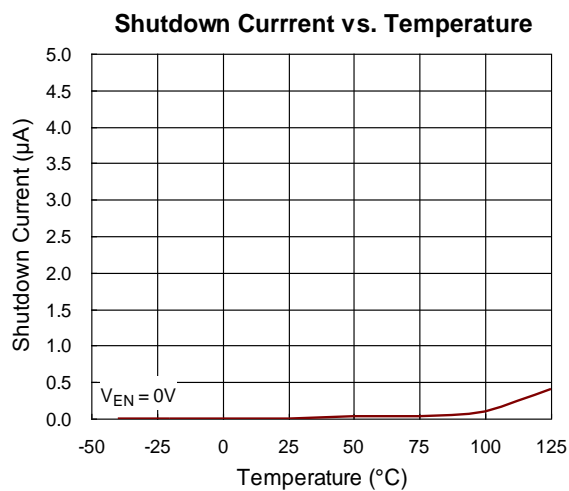
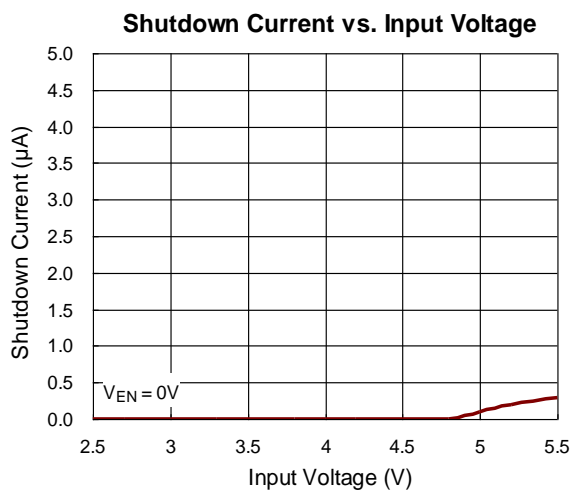
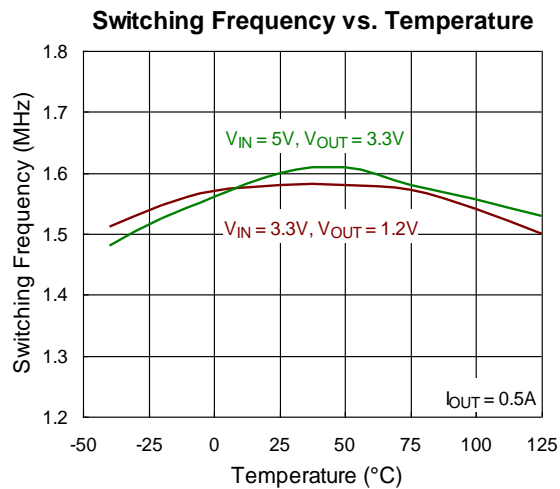
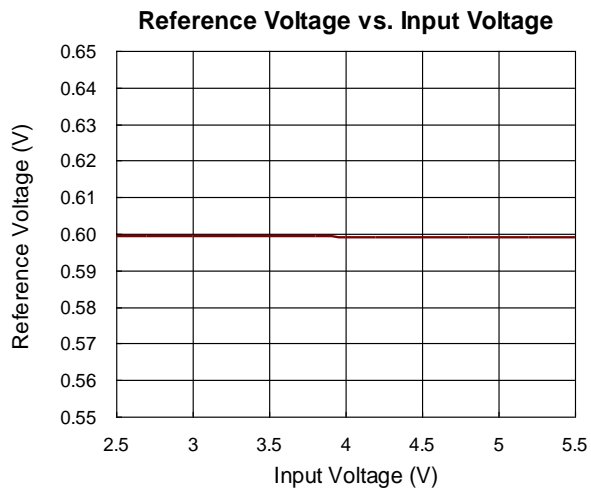
Note 4. The device is not guaranteed to function outside its operating conditions.

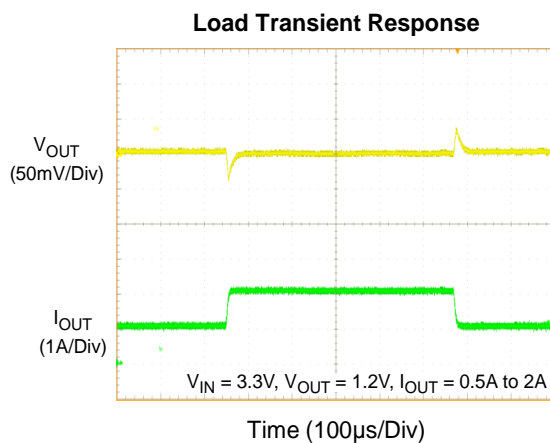
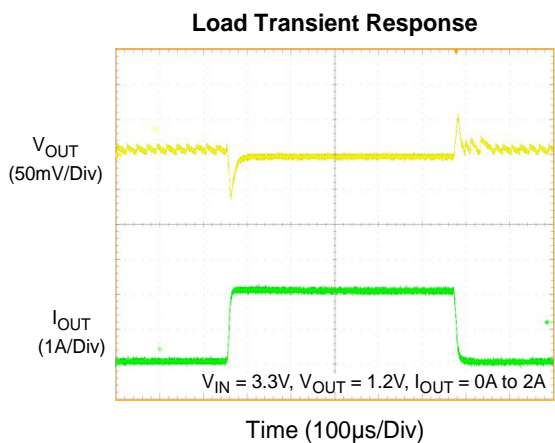
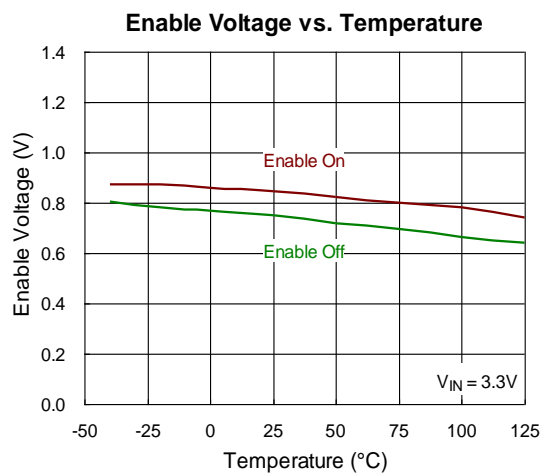
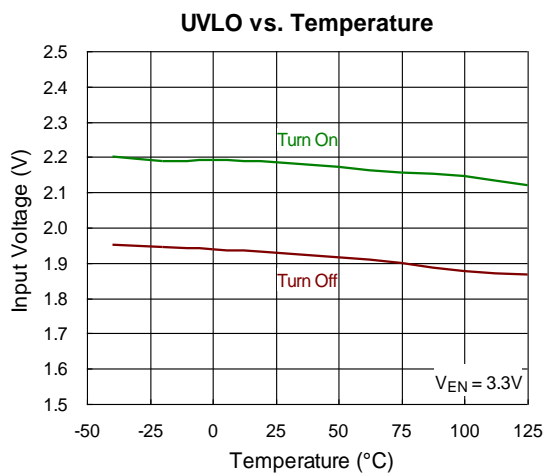
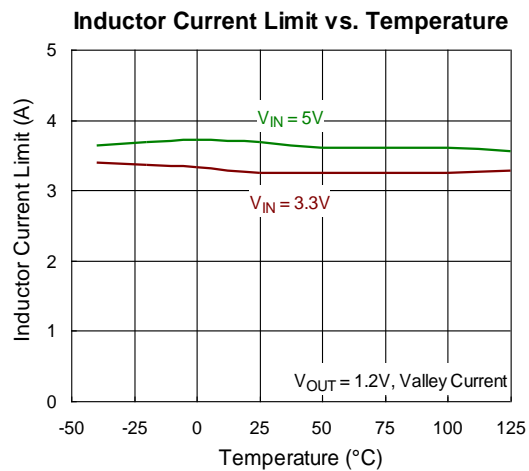
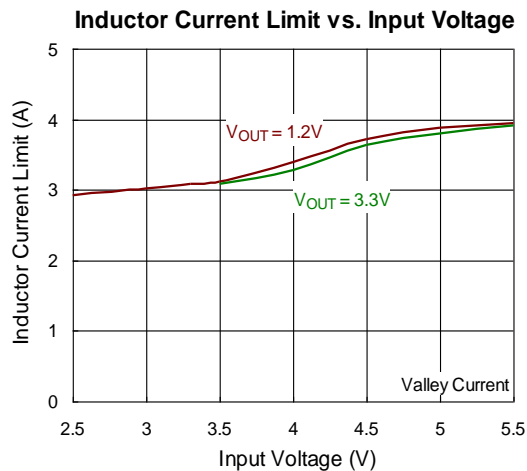
Typical Application Circuit

Table 1. Suggested Component Values

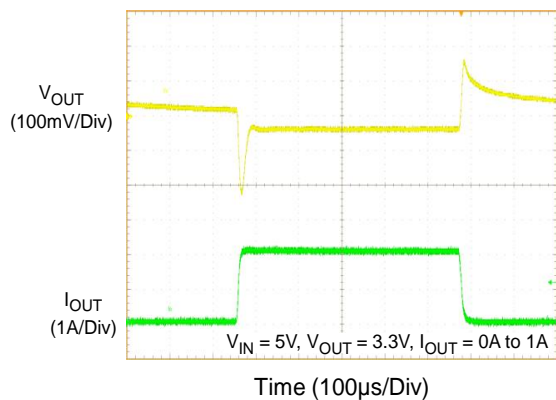
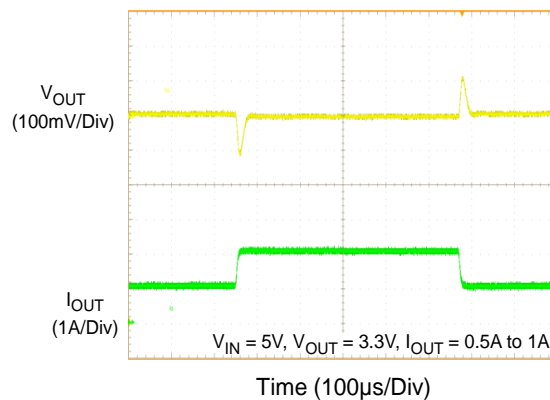
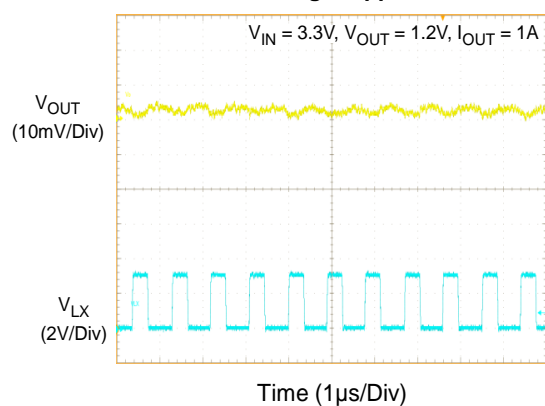
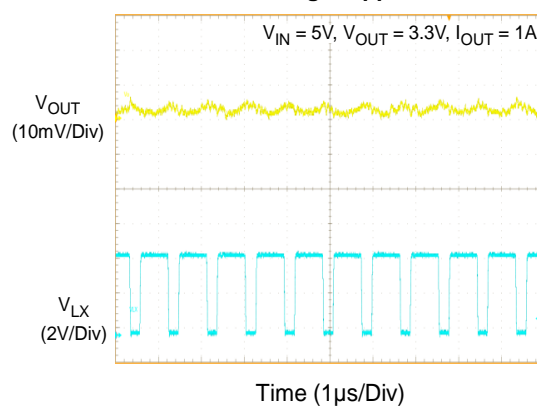
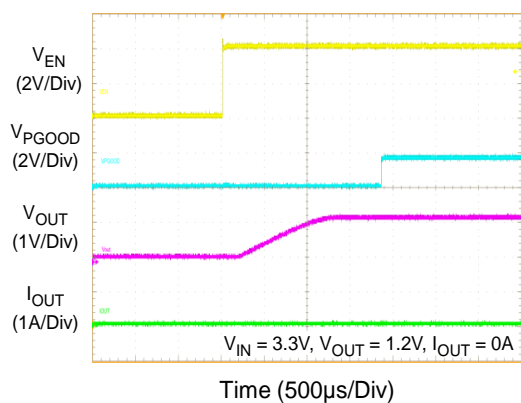
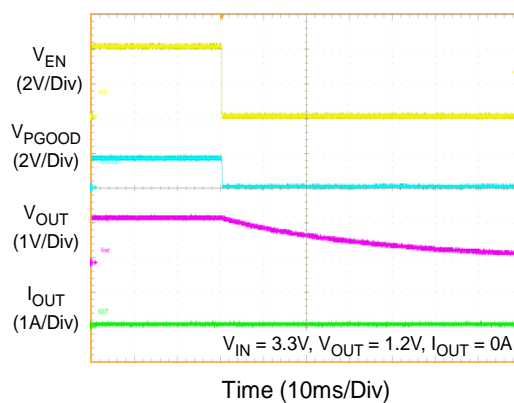
V _{OUT} (V)	R1 (kΩ)	R2 (kΩ)	C _{IN} (μF)	L (μH)	C _{OUT} (μF)
3.3	90	20	22	1.5	22
1.8	100	50	22	1.5	22
1.5	100	66.6	22	1.5	22
1.2	100	100	22	1.5	22
1.05	100	133	22	1.5	22
1	100	148	22	1.5	22

Typical Operating Characteristics

Efficiency vs. Output Current

Efficiency vs. Output Current

Output Voltage vs. Output Current

Output Voltage vs. Output Current

Output Voltage vs. Input Voltage

Output Voltage vs. Input Voltage






Load Transient Response

Load Transient Response

Voltage Ripple

Voltage Ripple

Power On from EN

Power Off from EN


Application Information

The HT8097A is a single-phase step-down converter. It provides single feedback loop constant on-time, current mode control with fast transient response. An internal 0.6V reference allows the output voltage to be precisely regulated for low output voltage applications. A fixed switching frequency (1MHz) oscillator and internal compensation are integrated to minimize external component count. Protection features include over current protection, under voltage protection and over temperature protection.

Output Voltage Setting

Connect a resistive voltage divider at the FB between V_{OUT} and GND to adjust the output voltage. The output voltage is set according to the following equation :

$$V_{OUT} = V_{REF} \times \left(1 + \frac{R1}{R2}\right)$$

where V_{REF} is the feedback reference voltage 0.6V (typ.).

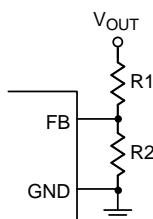


Figure 1. Setting V_{OUT} with a Voltage Divider

Chip Enable and Disable

The EN pin allows for power sequencing between the controller bias voltage and another voltage rail. The HT8097A remains in shutdown if the EN pin is lower than 400mV. When the EN pin rises above the V_{EN} trip point, the HT8097A begins a new initialization and soft-start cycle.

Internal Soft-Start

The HT8097A provides an internal soft-start function to prevent large inrush current and output voltage overshoot when the converter starts up. The soft-start (SS) automatically begins once the chip is enabled.

During soft-start, the internal soft-start capacitor becomes charged and generates a linear ramping up voltage across the capacitor. This voltage clamps the voltage at the FB pin, causing PWM pulse width to increase slowly and in turn reduce the input surge current. The internal 0.6V reference takes over the loop control once the internal ramping-up voltage becomes higher than 0.6V.

UVLO Protection

The HT8097A has input Under Voltage Lockout protection (UVLO). If the input voltage exceeds the UVLO rising threshold voltage (2.25V typ.), the converter resets and prepares the PWM for operation. If the input voltage falls below the UVLO falling threshold voltage during normal operation, the device will stop switching. The UVLO rising and falling threshold voltage has a hysteresis to prevent noise-caused reset.

Input Capacitor Selection

High quality ceramic input decoupling capacitor, such as X5R or X7R, with values greater than 22 μ F are recommended for the input capacitor. The X5R and X7R ceramic capacitors are usually selected for power regulator capacitors because the dielectric material has less capacitance variation and more temperature stability.

Voltage rating and current rating are the key parameters when selecting an input capacitor. Generally, selecting an input capacitor with voltage rating 1.5 times greater than the maximum input voltage is a conservatively safe design.

The input capacitor is used to supply the input RMS current, which can be approximately calculated using the following equation :

$$I_{IN_RMS} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)}$$

The next step is selecting a proper capacitor for RMS current rating. One good design uses more than one capacitor with low equivalent series resistance (ESR) in parallel to form a capacitor bank.

The input capacitance value determines the input ripple voltage of the regulator. The input voltage ripple can be approximately calculated using the following equation :

$$\Delta V_{IN} = \frac{I_{OUT(MAX)}}{C_{IN} \times f_{SW}} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Output Capacitor Selection

The output capacitor and the inductor form a low pass filter in the Buck topology. In steady state condition, the ripple current flowing into/out of the capacitor results in ripple voltage. The output voltage ripple (V_{P-P}) can be calculated by the following equation :

$$V_{P-P} = LIR \times I_{LOAD(MAX)} \times \left(ESR + \frac{1}{8 \times C_{OUT} \times f_{SW}}\right)$$

When load transient occurs, the output capacitor supplies the load current before the controller can respond. Therefore, the ESR will dominate the output voltage sag during load transient. The output voltage undershoot (V_{SAG}) can be calculated by the following equation :

$$V_{SAG} = \Delta I_{LOAD} \times ESR$$

For a given output voltage sag specification, the ESR value can be determined.

Another parameter that has influence on the output voltage sag is the equivalent series inductance (ESL). The rapid change in load current results in di/dt during transient. Therefore, the ESL contributes to part of the voltage sag. Using a capacitor with low ESL can obtain better transient performance. Generally, using several capacitors connected in parallel can have better transient performance than using a single capacitor for the same total ESR.

Inductor Selection

The switching frequency (on-time) and operating point (% ripple or LIR) determine the inductor value as shown below :

$$L = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{f_{SW} \times LIR \times I_{LOAD(MAX)} \times V_{IN}}$$

where LIR is the ratio of the peak-to-peak ripple current to the average inductor current.

Find a low loss inductor having the lowest possible DC resistance that fits in the allotted dimensions. The core

must be large enough not to saturate at the peak inductor current (I_{PEAK}) :

$$I_{PEAK} = I_{LOAD(MAX)} + \left(\frac{LIR}{2} \times I_{LOAD(MAX)}\right)$$

The calculation above serves as a general reference. To further improve transient response, the output inductor can be further reduced. This relation should be considered along with the selection of the output capacitor.

Inductor saturation current should be chosen over IC's current limit.

Thermal Considerations

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

where $T_{J(MAX)}$ is the maximum junction temperature, T_A is the ambient temperature, and θ_{JA} is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is 125°C. The junction to ambient thermal resistance, θ_{JA} , is layout dependent. For SOT-23-5 package, the thermal resistance, θ_{JA} , is 230.6°C/W on a standard four-layer thermal test board. For SOT-23-6 package, the thermal resistance, θ_{JA} , is 197.4°C/W on a standard four-layer thermal test board. The maximum power dissipation at $T_A = 25^\circ\text{C}$ can be calculated by the following formula :

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (230.6^\circ\text{C/W}) = 0.43\text{W for SOT-23-5 package}$$

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (197.4^\circ\text{C/W}) = 0.5\text{W for SOT-23-6 package}$$

The maximum power dissipation depends on the operating ambient temperature for fixed $T_{J(MAX)}$ and thermal resistance, θ_{JA} . The derating curve in Figure 2 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.

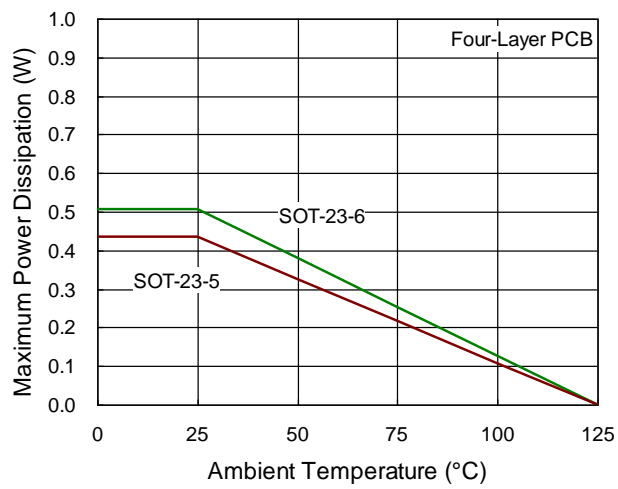
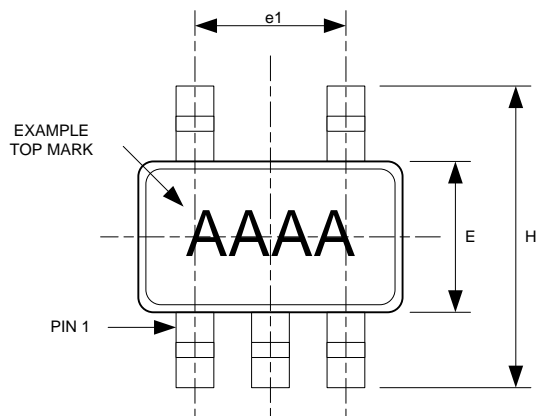


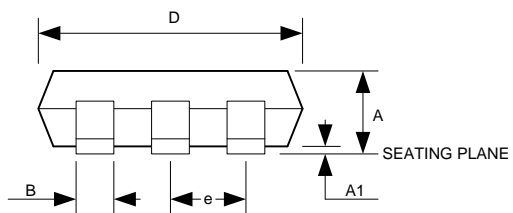
Figure 2. Derating Curve of Maximum Power Dissipation

PACKAGE DESCRIPTION

SOT23-5



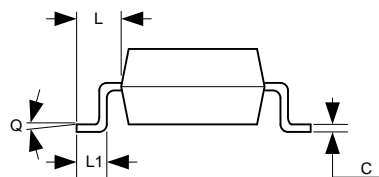
TOP VIEW



FRONT VIEW

5LD SOT-23 PACKAGE OUTLINE DIMENSIONS

Dimension	Min.	Max.
A	1.05	1.35
A1	0.04	0.15
B	0.3	0.5
C	0.09	0.2
D	2.8	3.0
H	2.5	3.1
E	1.5	1.7
e	0.95 REF.	
e1	1.90 REF.	
L1	0.2	0.55
L	0.35	0.8
Q	0°	10°



SIDE VIEW

NOTE:
 1.DIMENSIONS ARE IN MILLIMETERS
 2.DRAWING NOT TO SCALE
 3.DIMENSIONS ARE INCLUSIVE OF PLATING
 4.DIMENSIONS ARE EXCLUSIVE OF MOLD FLASH AND METAL BURR