

1. DESCRIPTION

The XH2576 series of regulators are monolithic integrated circuits that provide all the active functions for a step-down (buck) switching regulator, capable of driving 3-A load with excellent line and load regulation. These devices are available in fixed output voltages of 3.3 V, 5 V, 12 V, and an adjustable output version.

Requiring a minimum number of external components, these regulators are simple to use and include fault protection and a fixed-frequency oscillator.

The XH2576 series offers a high-efficiency replacement for popular three-terminal linear regulators. It substantially reduces the size of the heat sink, and in some cases no heat sink is required.

A standard series of inductors optimized for use with the XH2576 are available from several different manufacturers. This feature greatly simplifies the design of switch-mode power supplies.

Other features include a $\pm 4\%$ tolerance on output voltage within specified input voltages and output load conditions, and $\pm 10\%$ on the oscillator frequency. External shutdown is included, featuring 50- μ A (typical) standby current. The output switch includes cycle-by-cycle current limiting, as well as thermal shutdown for full protection under fault conditions.

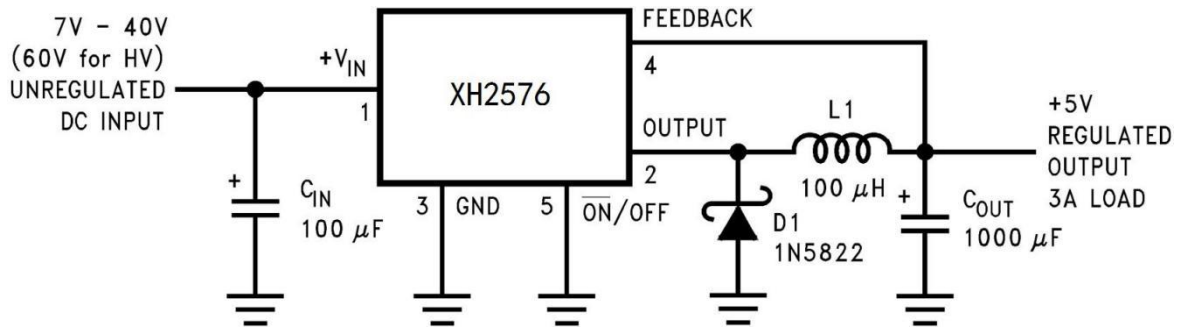
2. FEATURES

- 3.3-V, 5-V, 12-V, ADJ, and Adjustable Output Versions
- Adjustable Version Output Voltage Range, 1.23 V to 37 V $\pm 4\%$ Maximum Over Line and Load Conditions
- Specified 3-A Output Current
- Requires Only 4 External Components
- 52-kHz Fixed-Frequency Internal Oscillator
- TTL-Shutdown Capability, Low-Power Standby Mode
- High Efficiency
- Uses Readily Available Standard Inductors
- Create a Custom Design with WEBENCH Tools
- Thermal Shutdown and Current Limit Protection

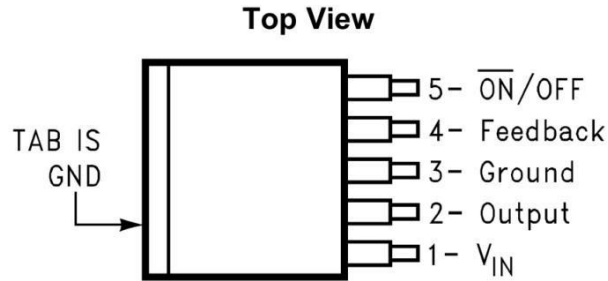
3. APPLICATIONS

- Simple High-Efficiency Step-Down (Buck) Regulator
- Efficient Preregulator for Linear Regulators
- On-Card Switching Regulators
- Positive-to-Negative Converter (Buck-Boost)

4. TYPICAL APPLICATION



5. PIN CONFIGURATION AND FUNCTIONS



Pin Functions

PIN NO.	NAME	I/O ⁽¹⁾	DESCRIPTION
1	V _{IN}	I	Supply input pin to collector pin of high-side transistor. Connect to power supply and input bypass capacitors C _{IN} . Path from V _{IN} pin to high frequency bypass C _{IN} and GND must be as short as possible.
2	OUTPUT	O	Emitter pin of the power transistor. This is a switching node. Attached this pin to an inductor and the cathode of the external diode.
3	GROUND	—	Ground pin. Path to C _{IN} must be as short as possible.
4	FEEDBACK	I	Feedback sense input pin. Connect to the midpoint of feedback divider to set V _{OUT} for ADJ version or connect this pin directly to the output capacitor for a fixed output version.
5	ON/OFF	I	Enable input to the voltage regulator. High = OFF and low = ON. Connect to GND to enable the voltage regulator. Do not leave this pin float.

(1) I = INPUT, O = OUTPUT

6. SPECIFICATIONS

6.1 Absolute Maximum Ratings

over the recommended operating junction temperature range of -40°C to 125°C (unless otherwise noted)⁽¹⁾

		MIN	MAX	UNIT
Maximum supply voltage	XH2576		45	V
ON /OFF pin input voltage		$-0.3V \leq V \leq +V_{IN}$		V
Output voltage to ground	(Steady-state)	-1		V
Power dissipation		Internally Limited		
Maximum junction temperature, T _j			150	°C
Storage temperature, T _{stg}		-65	150	°C

(1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

6.2 ESD Ratings

			VALUE	UNIT
V _(ESD)	Electrostatic discharge	Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ⁽¹⁾	±2000	V

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

6.3 Recommend Operating Conditions

over the recommended operating junction temperature range of -40°C to 125°C (unless otherwise noted)

		MIN	MAX	UNIT
Temperature	XH2576	-40	125	°C
Supply voltage	XH2576		40	V

6.4 Thermal Information

THERMAL METRIC		XH2576	UNIT
		TO-263	
R _{θJA}	Junction-to-ambient thermal resistance	42.6	°C/W
R _{θJC(top)}	Junction-to-case (top) thermal resistance	43.3	°C/W
R _{θJB}	Junction-to-board thermal resistance	22.4	°C/W
Ψ _{JT}	Junction-to-top characterization parameter	10.7	°C/W
Ψ _{JB}	Junction-to-board characterization parameter	21.3	°C/W
R _{θJC(bot)}	Junction-to-case (bottom) thermal resistance	0.4	°C/W

6.5 Electrical Characteristics : 3.3 V

Specifications are for $T_J = 25^\circ\text{C}$ (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SYSTEM PARAMETERS TEST CIRCUIT Figure 26 and Figure 32 ⁽¹⁾						
V_{OUT}	Output Voltage	$V_{IN} = 12\text{ V}$, $I_{LOAD} = 0.5\text{ A}$ Circuit of Figure 26 and Figure 32	3.234	3.3	3.366	V
	Output Voltage: XH2576	$6\text{ V} \leq V_{IN} \leq 40\text{ V}$, $0.5\text{ A} \leq I_{LOAD} \leq 3\text{ A}$ Circuit of Figure 26 and Figure 32	3.168	3.3	3.432	V
			3.135		3.465	
η	Efficiency	$V_{IN} = 12\text{ V}$, $I_{LOAD} = 3\text{ A}$	75%			

(1) External components such as the catch diode, inductor, input and output capacitors can affect switching regulator system performance. When the XH2576 is used as shown in [Figure 26](#) and [Figure 32](#), system performance is as shown in [Electrical Characteristics: All Output Voltage Versions](#).

6.6 Electrical Characteristics : 5 V

Specifications are for $T_J = 25^\circ\text{C}$ for the [Figure 26](#) and [Figure 32](#) (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SYSTEM PARAMETERS TEST CIRCUIT Figure 26 and Figure 32 ⁽¹⁾						
V_{OUT}	Output Voltage	$V_{IN} = 12\text{ V}$, $I_{LOAD} = 0.5\text{ A}$ Circuit of Figure 26 and Figure 32	4.9	5	5.1	V
V_{OUT}	Output Voltage XH2576	$0.5\text{ A} \leq I_{LOAD} \leq 3\text{ A}$, $8\text{ V} \leq V_{IN} \leq 40\text{ V}$ Circuit of Figure 26 and Figure 32	4.8	5	5.2	V
			4.75		5.25	
η	Efficiency	$V_{IN} = 12\text{ V}$, $I_{LOAD} = 3\text{ A}$	77%			

(1) External components such as the catch diode, inductor, input and output capacitors can affect switching regulator system performance. When the XH2576 is used as shown in [Figure 26](#) and [Figure 32](#), system performance is as shown in [Electrical Characteristics: All Output Voltage Versions](#).

6.7 Electrical Characteristics : 12 V

Specifications are for $T_J = 25^\circ\text{C}$ (unless otherwise noted).

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SYSTEM PARAMETERS TEST CIRCUIT Figure 26 and Figure 32 ⁽¹⁾						
V_{OUT}	Output Voltage	$V_{IN} = 25\text{ V}$, $I_{LOAD} = 0.5\text{ A}$ Circuit of Figure 26 and Figure 32	11.76	12	12.24	V
V_{OUT}	Output Voltage XH2576	$0.5\text{ A} \leq I_{LOAD} \leq 3\text{ A}$, $15\text{ V} \leq V_{IN} \leq 40\text{ V}$ Circuit of Figure 26 and Figure 32 and	11.52	12	12.48	V
			11.4		12.6	
η	Efficiency	$V_{IN} = 15\text{ V}$, $I_{LOAD} = 3\text{ A}$	88%			

(1) External components such as the catch diode, inductor, input and output capacitors can affect switching regulator system performance. When the XH2576 is used as shown in [Figure 26](#) and [Figure 32](#), system performance is as shown in [Electrical Characteristics: All Output Voltage Versions](#).

6.8 Electrical Characteristics : Adjustable Output Voltage

over operating free-air temperature range (unless otherwise noted).

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
SYSTEM PARAMETERS TEST CIRCUIT Figure 26 and Figure 32 ⁽¹⁾					
V _{OUT} Feedback voltage	V _{IN} = 12 V, I _{LOAD} = 0.5 A V _{OUT} = 5 V, Circuit of Figure 26 and Figure 32	1.217	1.23	1.243	V
V _{OUT} Feedback Voltage XH2576	0.5 A ≤ I _{LOAD} ≤ 3 A, 8 V ≤ V _{IN} ≤ 40 V V _{OUT} = 5 V, Circuit of Figure 26 and Figure 32	1.193	1.23	1.267	V
	T _J = 25°C Applies over full operating temperature range	1.18		1.28	
η Efficiency	V _{IN} = 12 V, I _{LOAD} = 3 A, V _{OUT} = 5 V	77%			

(1) External components such as the catch diode, inductor, input and output capacitors can affect switching regulator system performance. When the XH2576 is used as shown in [Figure 26](#) and [Figure 32](#), system performance is as shown in [Electrical Characteristics: All Output Voltage Versions](#).

6.9 Electrical Characteristics: All Output Voltage Versions

over operating free-air temperature range (unless otherwise noted)

PARAMETER	TEST CONDITIONS	MIN	TYP ⁽¹⁾	MAX	UNIT
SYSTEM PARAMETERS TEST CIRCUIT Figure 26 and Figure 32 ⁽²⁾					
I _b Feedback Bias Current	V _{OUT} = 5 V (Adjustable Version Only)	T _J = 25°C	100	50	nA
		Applies over full operating temperature range	500		
f _o Oscillator Frequency ⁽³⁾	T _J = 25°C	47	52	58	kHz
	Applies over full operating temperature range	42		63	

- (1) All limits specified at room temperature (25°C) unless otherwise noted. All room temperature limits are 100% production tested. All limits at temperature extremes are specified through correlation using standard Statistical Quality Control (SQC) methods.
- (2) External components such as the catch diode, inductor, input and output capacitors can affect switching regulator system performance. When the XH2576 is used as shown in [Figure 26](#) and [Figure 32](#), system performance is as shown in [Electrical Characteristics: All Output Voltage Versions](#).
- (3) The oscillator frequency reduces to approximately 11 kHz in the event of an output short or an overload which causes the regulated output voltage to drop approximately 40% from the nominal output voltage. This self protection feature lowers the average power dissipation of the IC by lowering the minimum duty cycle from 5% down to approximately 2%.

Electrical Characteristics: All Output Voltage Versions (continued)

over operating free-air temperature range (unless otherwise noted)

PARAMETER		TEST CONDITIONS		MIN	TYP ⁽¹⁾	MAX	UNIT
V _{SAT}	Saturation Voltage	I _{OUT} = 3 A ⁽⁴⁾	T _J = 25°C	1.4		1.8	V
			Applies over full operating temperature range	2			
DC	Max Duty Cycle (ON) ⁽⁵⁾			93%	98%		
I _{CL}	Current Limit ⁽⁴⁾⁽³⁾	T _J = 25°C		4.2	5.8	6.9	A
		Applies over full operating temperature range		3.5	7.5		
I _L	Output Leakage Current	Output = 0 V Output = -1 V Output = -1 V ⁽⁶⁾⁽⁷⁾		2	7.5	30	mA
I _Q	Quiescent Current ⁽⁶⁾			5		10	mA
I _{STBY}	Standby Quiescent Current	$\overline{\text{ON}}$ /OFF Pin = 5 V (OFF)		50		200	μA
$\overline{\text{ON}}$ /OFF CONTROL TEST CIRCUIT Figure 26 and Figure 32							
V _{IH}	$\overline{\text{ON}}$ /OFF Pin Logic Input Level	V _{OUT} = 0 V	T _J = 25°C	2.2	1.4		V
			Applies over full operating temperature range	2.4			
V _{IL}	$\overline{\text{ON}}$ /OFF Pin Logic Input Level	V _{OUT} = Nominal Output Voltage	T _J = 25°C	1.2			V
			Applies over full operating temperature range	0.8			
I _{IH}	$\overline{\text{ON}}$ /OFF Pin Input Current	$\overline{\text{ON}}$ /OFF Pin = 5 V (OFF)		12		30	μA
I _{IL}		$\overline{\text{ON}}$ /OFF Pin = 0 V (ON)		0		10	μA

(4) Output pin sourcing current. No diode, inductor or capacitor connected to output.

(5) Feedback pin removed from output and connected to 0V.

(6) Feedback pin removed from output and connected to +12 V for the Adjustable, 3.3-V, and 5-V versions, and +25 V for the 12-V and 15-V versions, to force the output transistor OFF.

(7) V_{IN} = 40 V

6.10 Typical Characteristics

(Circuit of Figure 26 and Figure 32)

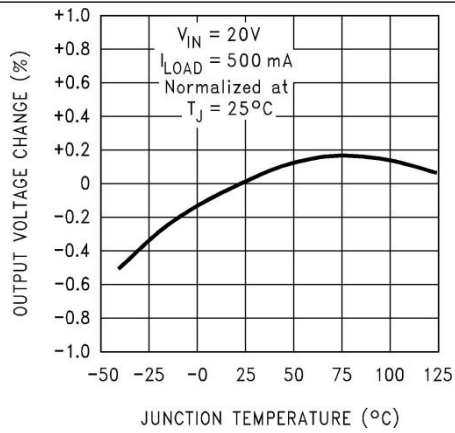


Figure 1. Normalized Output Voltage

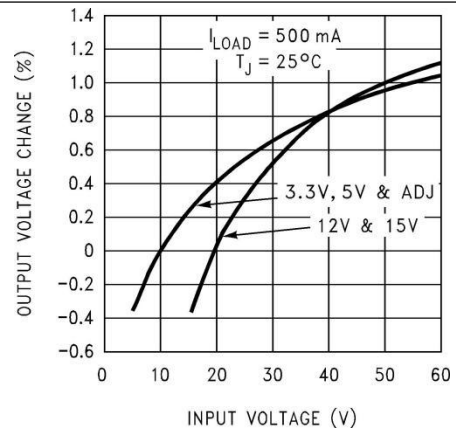


Figure 2. Line Regulation

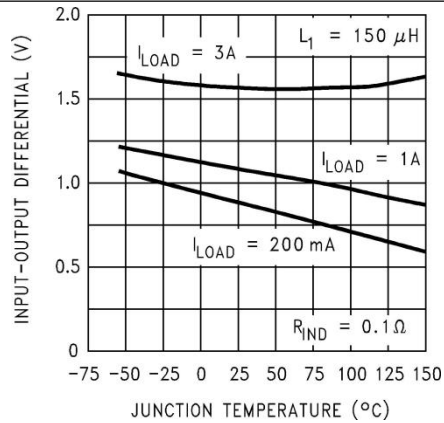


Figure 3. Dropout Voltage

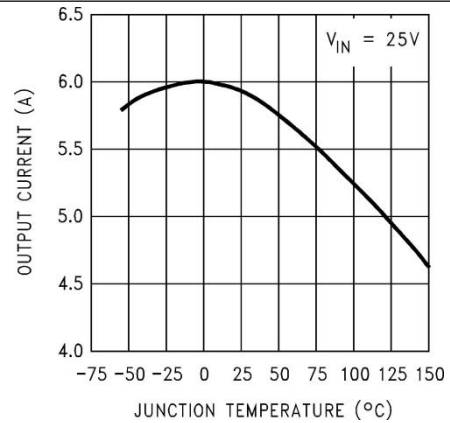


Figure 4. Current Limit

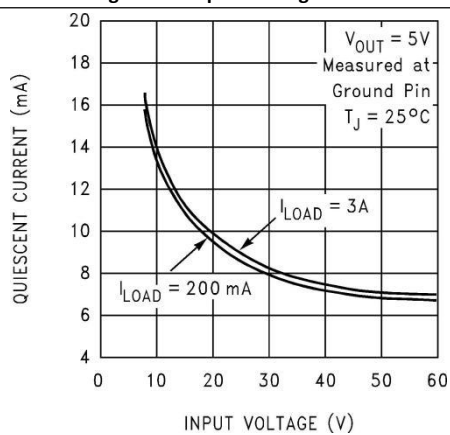


Figure 5. Quiescent Current

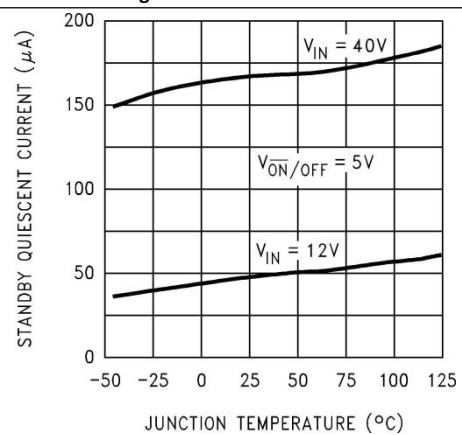


Figure 6. Standby Quiescent Current

Typical Characteristics(continued)

(Circuit of Figure 26 and Figure 32)

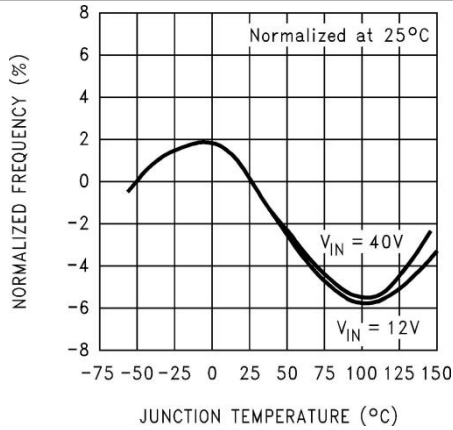


Figure 7. Oscillator Frequency

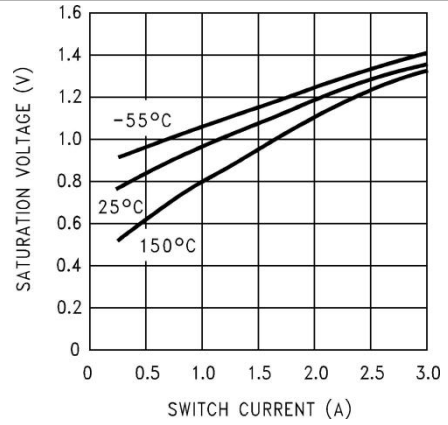


Figure 8. Switch Saturation Voltage

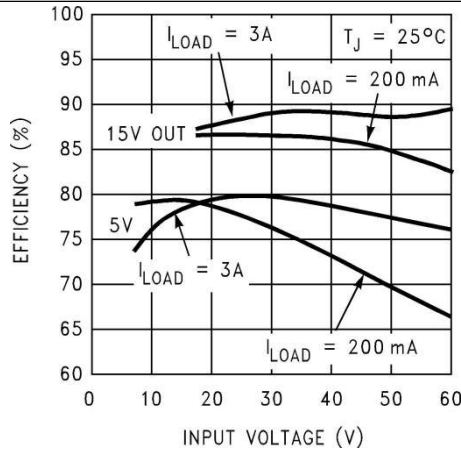


Figure 9. Efficiency

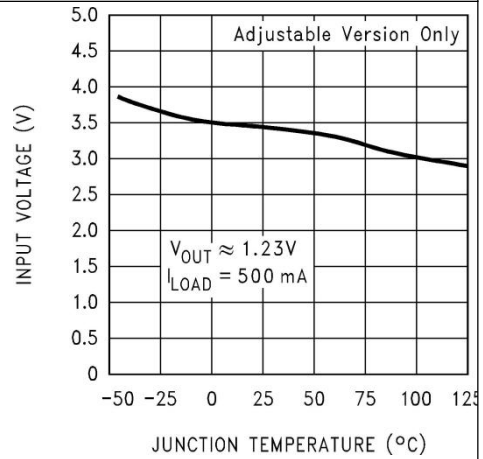


Figure 10. Minimum Operating Voltage

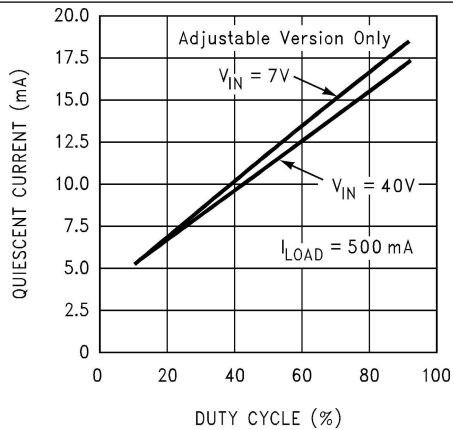


Figure 11. Quiescent Current vs Duty Cycle

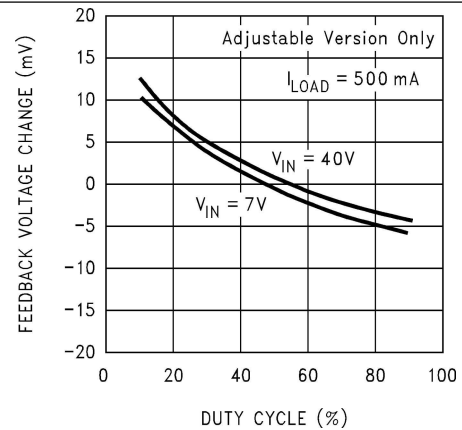


Figure 12. Feedback Voltage vs Duty Cycle

Typical Characteristics(continued)

(Circuit of Figure 26 and Figure 32)

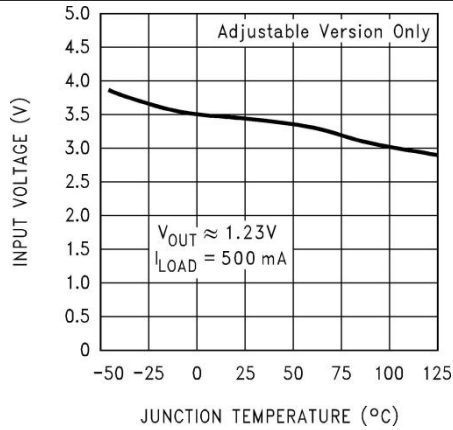


Figure 13. Minimum Operating Voltage

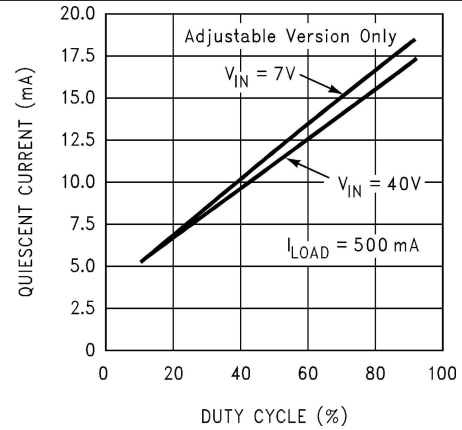


Figure 14. Quiescent Current vs Duty Cycle

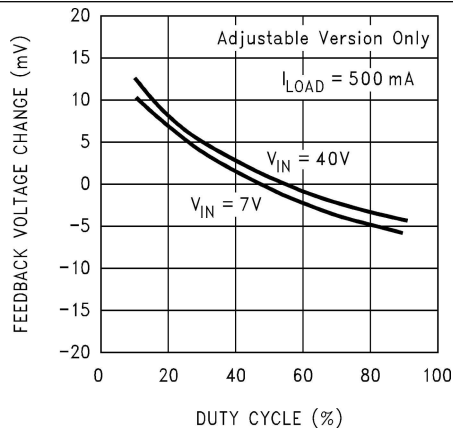


Figure 15. Feedback Voltage vs Duty Cycle

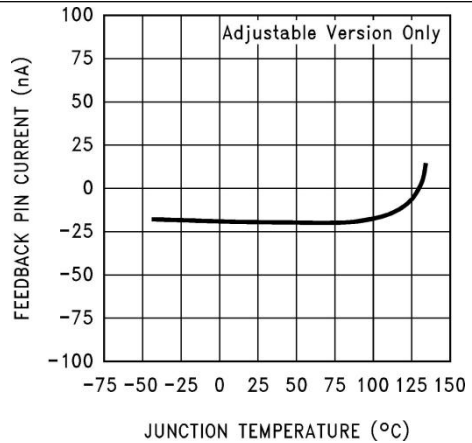
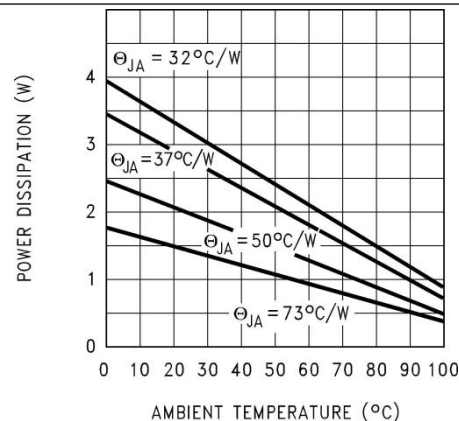
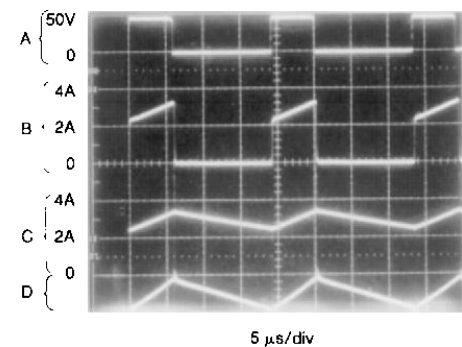


Figure 16. Feedback Pin Current



If the TO-263 package is used, the thermal resistance can be reduced by increasing the PCB copper area thermally connected to the package. Using 0.5 square inches of copper area, θ_{JA} is 50°C/W, with 1 square inch of copper area, θ_{JA} is 37°C/W, and with 1.6 or more square inches of copper area, θ_{JA} is 32°C/W.

Figure 17. Maximum Power Dissipation (DDPAK/TO-263)



$V_{OUT} = 15V$
A: Output Pin Voltage, 50 V/div
B: Output Pin Current, 2 A/div
C: Inductor Current, 2 A/div
D: Output Ripple Voltage, 50 mV/div, AC-Coupled
Horizontal Time Base: 5 μ s/div

Figure 18. Switching Waveforms

Typical Characteristics(continued)

(Circuit of [Figure 26](#) and [Figure 32](#))

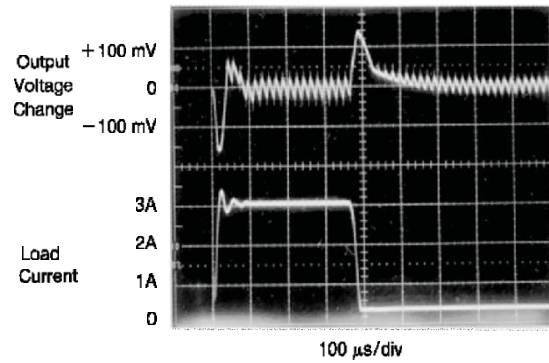


Figure 19. Load Transient Response

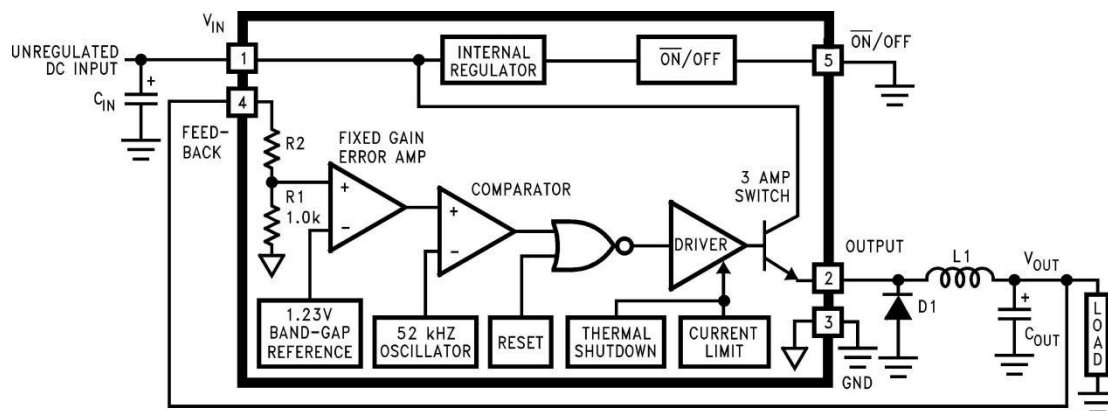
7. DETAILED DESCRIPTION

7.1 Overview

The XH2576 SIMPLE SWITCHER regulator is an easy-to-use, non-synchronous step-down DC-DC delivering up to 3-A DC load current with excellent line and load regulation.

These devices are available in fixed output voltages of 3.3 V, 5 V, 12 V, ADJ, and an adjustable output version. The family requires few external components, and the pin arrangement was designed for simple, optimum PCB layout.

7.2 Functional Block Diagram



3.3 V R2 = 1.7 k
5 V, R2 = 3.1 k
12 V, R2 = 8.84 k
For ADJ. Version
R1 = Open, R2 = 0 Ω

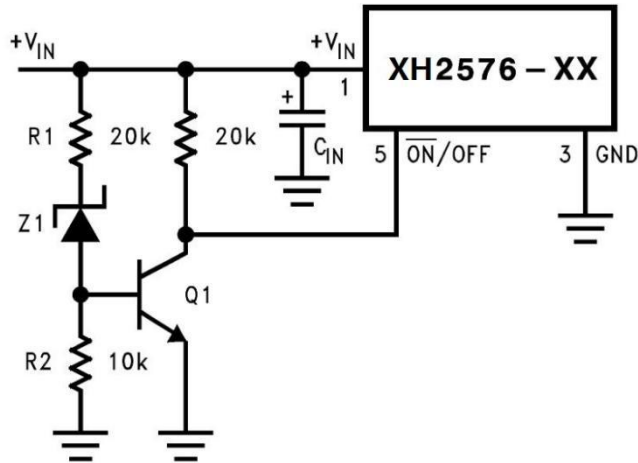
7.3 Feature Description

7.3.1 Undervoltage Lockout

In some applications it is desirable to keep the regulator off until the input voltage reaches a certain threshold. Figure 20 shows an undervoltage lockout circuit that accomplishes this task, while Figure 21 shows the same circuit applied to a buck-boost configuration. These circuits keep the regulator off until the input voltage reaches a predetermined level.

$$V_{TH} \approx V_{Z1} + 2V_{BE}(Q1)$$

Feature Description (continued)



Complete circuit not shown.

Figure 20. Undervoltage Lockout for Buck Circuit

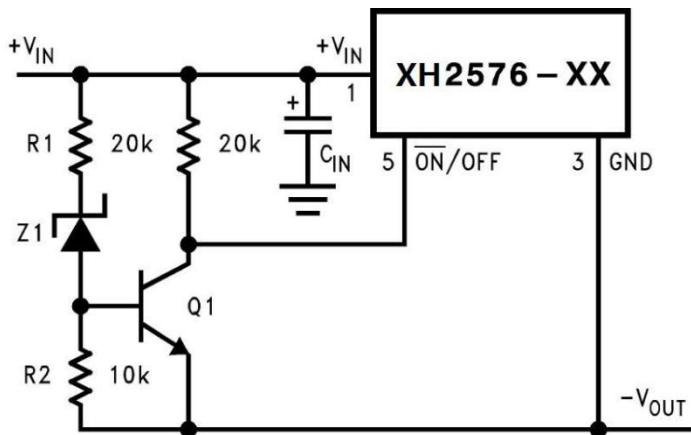


Figure 21. Undervoltage Lockout for Buck-Boost Circuit

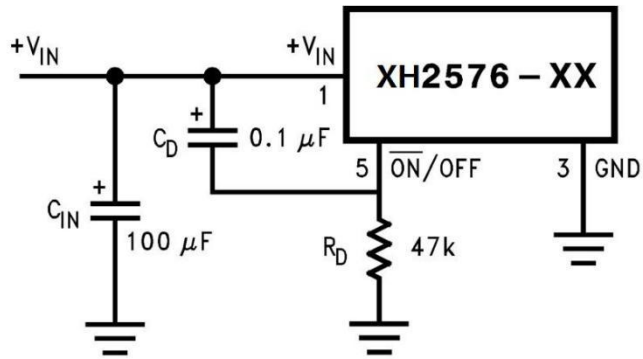
7.3.2 Delayed Start-Up

The $\overline{\text{ON}}/\text{OFF}$ pin can be used to provide a delayed start-up feature as shown in Figure 22. With an input voltage of 20 V and for the part values shown, the circuit provides approximately 10 ms of delay time before the circuit begins switching. Increasing the RC time constant can provide longer delay times. But excessively large RC time constants can cause problems with input voltages that are high in 60-Hz or 120-Hz ripple, by coupling the ripple into the $\overline{\text{ON}}/\text{OFF}$ pin.

7.3.3 Adjustable Output, Low-Ripple Power Supply

Figure 23 shows a 3-A power supply that features an adjustable output voltage. An additional LC filter that reduces the output ripple by a factor of 10 or more is included in this circuit.

Feature Description (continued)



Complete circuit not shown.

Figure 22. Delayed Start-Up

7.4 Device Functional Modes

7.4.1 Shutdown Mode

The $\overline{\text{ON/OFF}}$ pin provides electrical $\overline{\text{ON}}$ and OFF control for the XH2576. When the voltage of this pin is higher than 1.4 V, the device is in shutdown mode. The typical standby current in this mode is 50 μA .

7.4.2 Active Mode

When the voltage of the $\overline{\text{ON/OFF}}$ pin is below 1.2 V, the device starts switching, and the output voltage rises until it reaches the normal regulation voltage.

7.4.3 Current Limit

The XH2576 device has current limiting to prevent the switch current from exceeding safe values during an accidental overload on the output. This current limit value can be found in Electrical Characteristics: All Output Voltage Versions under the heading of ICL.

The XH2576 uses cycle-by-cycle peak current limit for overload protection. This helps to prevent damage to the device and external components. The regulator operates in current limit mode whenever the inductor current exceeds the value of ICL given in Electrical Characteristics: All Output Voltage Versions. This occurs if the load current is greater than 3 A, or the converter is starting up. Keep in mind that the maximum available load current depends on the input voltage, output voltage, and inductor value. The regulator also incorporates short-circuit protection to prevent inductor current run-away. When the voltage on the FB pin (ADJ) falls below about 0.58 V the switching frequency is dropped to about 11 kHz. This allows the inductor current to ramp down sufficiently during the switch OFF-time to prevent saturation.

8. APPLICATION AND IMPLEMENTATION

NOTE

Information in the following applications sections is not part of the Xinluda component specification, and Xinluda does not warrant its accuracy or completeness. Xinluda's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

8.1 Application Information

8.1.1 Input Capacitor (C_{IN})

To maintain stability, the regulator input pin must be bypassed with at least a 100- μ F electrolytic capacitor. The capacitor's leads must be kept short, and placed near the regulator.

If the operating temperature range includes temperatures below -25°C , the input capacitor value may need to be larger. With most electrolytic capacitors, the capacitance value decreases and the ESR increases with lower temperatures and age. Paralleling a ceramic or solid tantalum capacitor increases the regulator stability at cold temperatures. For maximum capacitor operating lifetime, the RMS ripple current rating of the capacitor must be greater than:

$$1.2 \times \left(\frac{t_{ON}}{T} \right) \times I_{LOAD}$$

$$\text{where } \frac{t_{ON}}{T} = \frac{V_{OUT}}{V_{IN}} \text{ for a buck regulator}$$

$$\text{and } \frac{t_{ON}}{T} = \frac{|V_{OUT}|}{|V_{OUT}| + V_{IN}} \text{ for a buck-boost regulator.}$$

8.1.2 Inductor Selection

All switching regulators have two basic modes of operation: continuous and discontinuous. The difference between the two types relates to the inductor current, whether it is flowing continuously, or if it drops to zero for a period of time in the normal switching cycle. Each mode has distinctively different operating characteristics, which can affect the regulator performance and requirements.

The XH2576 (or any of the SIMPLE SWITCHER family) can be used for both continuous and discontinuous modes of operation.

The inductor value selection guides in Figure 27 through Figure 31 are designed for buck regulator designs of the continuous inductor current type. When using inductor values shown in the inductor selection guide, the peak-to-peak inductor ripple current is approximately 20% to 30% of the maximum DC current. With relatively heavy load currents, the circuit operates in the continuous mode (inductor current always flowing), but under light load conditions, the circuit is forced to the discontinuous mode (inductor current falls to zero for a period of time). This discontinuous mode of operation is perfectly acceptable. For light loads (less than approximately 300 mA), it may be desirable to operate the regulator in the discontinuous mode, primarily because of the lower

inductor values required for the discontinuous mode.

The selection guide chooses inductor values suitable for continuous mode operation, but if the inductor value chosen is prohibitively high, the designer should investigate the possibility of discontinuous operation.

Inductors are available in different styles such as pot core, toriod, E-frame, bobbin core, and so on, as well as different core materials, such as ferrites and powdered iron. The bobbin core is the least expensive type, and consists of wire wrapped on a ferrite rod core. This type of construction makes for an inexpensive inductor; however, because the magnetic flux is not completely contained within the core, the bobbin core generates more electromagnetic interference (EMI). This EMI can cause problems in sensitive circuits, or can give incorrect scope readings because of induced voltages in the scope probe.

The inductors listed in the selection chart include ferrite pot core construction for AIE, powdered iron toroid for Pulse Engineering, and ferrite bobbin core for Renco.

8.1.3 Inductor Ripple Current

When the switcher is operating in the continuous mode, the inductor current waveform ranges from a triangular to a sawtooth type of waveform (depending on the input voltage). For a given input voltage and output voltage, the peak-to-peak amplitude of this inductor current waveform remains constant. As the load current rises or falls, the entire sawtooth current waveform also rises or falls. The average DC value of this waveform is equal to the DC load current (in the buck regulator configuration).

If the load current drops to a low enough level, the bottom of the sawtooth current waveform reaches zero, and the switcher changes to a discontinuous mode of operation. This is a perfectly acceptable mode of operation. Any buck switching regulator (no matter how large the inductor value is) is forced to run discontinuous if the load current is light enough.

8.1.4 Output Capacitor

An output capacitor is required to filter the output voltage and is needed for loop stability. The capacitor must be placed near the XH2576 using short PCB traces. Standard aluminum electrolytics are usually adequate, but recommends low ESR types for low output ripple voltage and good stability. The ESR of a capacitor depends on many factors, including: the value, the voltage rating, physical size, and the type of construction. In general, low value or low voltage (less than 12 V) electrolytic capacitors usually have higher ESR numbers.

The amount of output ripple voltage is primarily a function of the ESR (Equivalent Series Resistance) of the output capacitor and the amplitude of the inductor ripple current (ΔI_{IND}). See [Inductor Ripple Current](#).

The lower capacitor values (220 μ F to 1000 μ F) allows typically 50 mV to 150 mV of output ripple voltage, while larger-value capacitors reduces the ripple to approximately 20 mV to 50 mV.

Output Ripple Voltage = (ΔI_{IND}) (ESR of C_{OUT})

To further reduce the output ripple voltage, several standard electrolytic capacitors may be paralleled, or a higher-grade capacitor may be used. Such capacitors are often called *high-*

frequency, low-inductance, or low-ESR. These reduces the output ripple to 10 mV or 20 mV. However, when operating in the continuous mode, reducing the ESR below $0.03\ \Omega$ can cause instability in the regulator.

Tantalum capacitors can have a very low ESR, and must be carefully evaluated if it is the only output capacitor. Because of their good low temperature characteristics, a tantalum can be used in parallel with aluminum electrolytics, with the tantalum making up 10% or 20% of the total capacitance.

The ripple current rating of the capacitor at 52 kHz should be at least 50% higher than the peak-to-peak inductor ripple current.

8.1.5 Catch Diode

Buck regulators require a diode to provide a return path for the inductor current when the switch is off. This diode must be placed close to the XH2576 using short leads and short printed-circuit traces.

Because of their fast switching speed and low forward voltage drop, Schottky diodes provide the best efficiency, especially in low output voltage switching regulators (less than 5 V). Fast-recovery, high-efficiency, or ultra-fast recovery diodes are also suitable, but some types with an abrupt turnoff characteristic may cause instability and EMI problems. A fast-recovery diode with soft recovery characteristics is a better choice. Standard 60-Hz diodes (for example, 1N4001 or 1N5400, and so on) are also not suitable. See Table 3 for Schottky and soft fast-recovery diode selection guide.

8.1.6 Output Voltage Ripple and Transients

The output voltage of a switching power supply contains a sawtooth ripple voltage at the switcher frequency, typically about 1% of the output voltage, and may also contain short voltage spikes at the peaks of the sawtooth waveform.

The output ripple voltage is due mainly to the inductor sawtooth ripple current multiplied by the ESR of the output capacitor (see Inductor Selection).

The voltage spikes are present because of the fast switching action of the output switch, and the parasitic inductance of the output filter capacitor. To minimize these voltage spikes, special low inductance capacitors can be used, and their lead lengths must be kept short. Wiring inductance, stray capacitance, as well as the scope probe used to evaluate these transients, all contribute to the amplitude of these spikes.

An additional small LC filter (20 μH and 100 μF) can be added to the output (as shown in Figure 23) to further reduce the amount of output ripple and transients. A 10 $\times$ reduction in output ripple voltage and transients is possible with this filter.

8.1.7 Feedback Connection

The XH2576 (fixed voltage versions) feedback pin must be wired to the output voltage point of the switching power supply. When using the adjustable version, physically locate both output voltage programming resistors near the XH2576 to avoid picking up unwanted noise. Avoid using resistors greater than 100 k Ω because of the increased chance of noise pickup.

8.1.8 ON /OFF INPUT

For normal operation, the $\overline{\text{ON}}$ /OFF pin must be grounded or driven with a low-level TTL voltage (typically below 1.6 V). To put the regulator into standby mode, drive this pin with a high-level TTL or CMOS signal. The ON/OFF pin can be safely pulled up to $+V_{\text{IN}}$ without a resistor in series with it. The ON /OFF pin must not be left open.

8.1.9 Inverting Regulator

Figure 24 shows a XH2576-12 in a buck-boost configuration to generate a negative 12-V output from a positive input voltage. This circuit bootstraps the ground pin of the regulator to the negative output voltage, then by grounding the feedback pin, the regulator senses the inverted output voltage and regulates it to -12 V.

For an input voltage of 12 V or more, the maximum available output current in this configuration is approximately 700 mA. At lighter loads, the minimum input voltage required drops to

approximately 4.7 V.

The switch currents in this buck-boost configuration are higher than in the standard buck-mode design, thus lowering the available output current. Also, the start-up input current of the buck-boost converter is higher than the standard buck-mode regulator, and this may overload an input power source with a current limit less than

5 A. Using a delayed turn-on or an undervoltage lockout circuit (described in [Negative Boost Regulator](#)) would allow the input voltage to rise to a high enough level before the switcher would be allowed to turn on.

Because of the structural differences between the buck and the buck-boost regulator topologies, the buck regulator design procedure section can not be used to select the inductor or the output capacitor. The recommended range of inductor values for the buck-boost design is between 68 μH and 220 μH , and the output capacitor values must be larger than what is normally required for buck designs. Low input voltages or high output currents require a large value output capacitor (in the thousands of micro Farads).

The peak inductor current, which is the same as the peak switch current, can be calculated in [Equation 4](#):

$$I_p \approx \frac{I_{\text{LOAD}} (V_{\text{IN}} + |V_{\text{O}}|)}{V_{\text{IN}}} + \frac{V_{\text{IN}} |V_{\text{O}}|}{V_{\text{IN}} + |V_{\text{O}}|} \times \frac{1}{2L_1 f_{\text{osc}}}$$

where

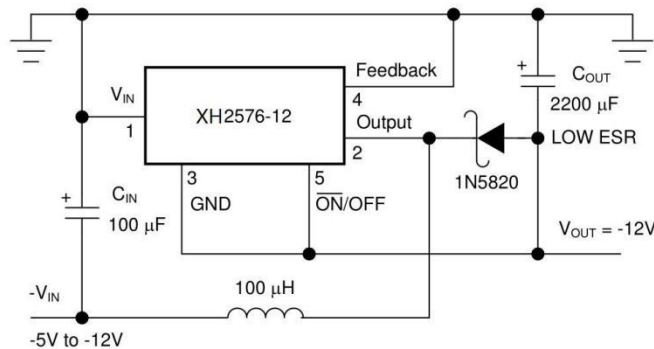
- $f_{\text{osc}} = 52 \text{ kHz}$

Under normal continuous inductor current operating conditions, the minimum V_{IN} represents the worst case. Select an inductor that is rated for the peak current anticipated.

8.1.10 Negative Boost Regulator

Another variation on the buck-boost topology is the negative boost configuration. The circuit in Figure 25 accepts an input voltage ranging from -5 V to -12 V and provides a regulated -12-V output. Input voltages greater than

-12 V causes the output to rise above -12 V, but does not damage the regulator.



Typical Load Current
400 mA for $V_{\text{IN}} = -5.2 \text{ V}$
750 mA for $V_{\text{IN}} = -7 \text{ V}$
Heat sink may be required.

Figure 25. Negative Boost

Because of the boosting function of this type of regulator, the switch current is relatively high, especially at low input voltages. Output load current limitations are a result of the maximum current rating of the switch. Also, boost regulators can not provide current-limiting load protection in the event of a shorted load, so some other means (such as a fuse) may be necessary.

9. POWER SUPPLY RECOMMENDATIONS

As in any switching regulator, layout is very important. Rapidly switching currents associated with wiring inductance generate voltage transients which can cause problems. For minimal inductance and ground loops, the length of the leads indicated by heavy lines should be kept as short as possible. Single-point grounding (as indicated) or ground plane construction should be used for best results. When using the adjustable version, physically locate the programming resistors near the regulator, to keep the sensitive feedback wiring short.

10. LAYOUT

10.1 Layout Guidelines

Board layout is critical for the proper operation of switching power supplies. First, the ground plane area must be sufficient for thermal dissipation purposes. Second, appropriate guidelines must be followed to reduce the effects of switching noise. Switch mode converters are very fast switching devices. In such cases, the rapid increase of input current combined with the parasitic trace inductance generates unwanted $L di/dt$ noise spikes. The magnitude of this noise tends to increase as the output current increases. This noise may turn into electromagnetic interference (EMI) and can also cause problems in device performance. Therefore, take care in layout to minimize the effect of this switching noise. The most important layout rule is to keep the AC current loops as small as possible. Figure 33 shows the current flow in a buck converter. The top schematic shows a dotted line which represents the current flow during the top-switch ON-state. The middle schematic shows the current flow during the top-switch OFF-state. The bottom schematic shows the currents referred to as AC currents. These AC currents are the most critical because they are changing in a very short time period. The dotted lines of the bottom schematic are the traces to keep as short and wide as possible. This also yields a small loop area reducing the loop inductance. To avoid functional problems due to layout, review the PCB layout example. Best results are achieved if the placement of the XH2576 device, the bypass capacitor, the Schottky diode, RFBB, RFBT, and the inductor are placed .also recommends using 2-oz copper boards or heavier to help thermal dissipation and to reduce the parasitic inductances of board traces. See application note AN-1229 SIMPLE SWITCHER PCB Layout Guidelines (SNVA054) for more information.

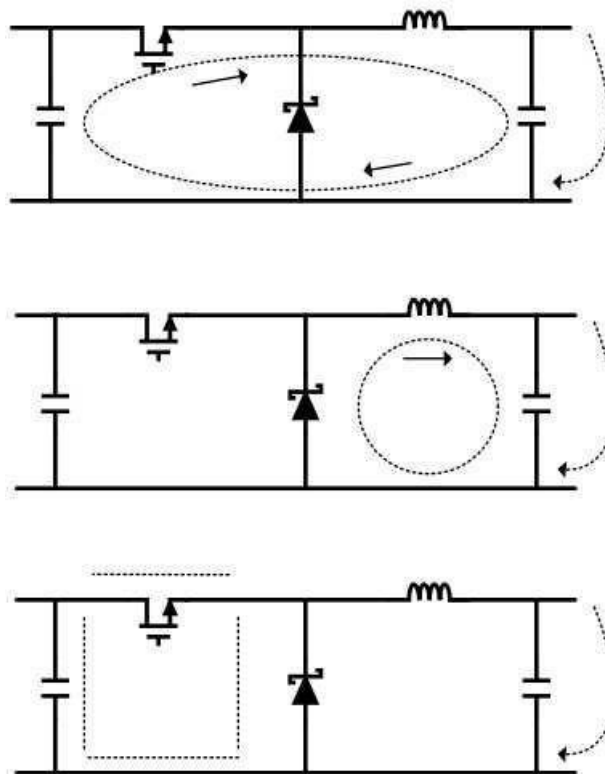


Figure 26. Current Flow in Buck Application

10.2 Grounding

To maintain output voltage stability, the power ground connections must be low-impedance (see Figure 26 and Figure 32). For the TO-263 style package, both the tab and pin 3 are ground and either connection may be used, as they are both part of the same copper lead frame.

10.3 Heat Sink and Thermal Considerations

In many cases, only a small heat sink is required to keep the XH2576 junction temperature within the allowed operating range. For each application, to determine whether or not a heat sink is required, the following must be identified:

1. Maximum ambient temperature (in the application).
2. Maximum regulator power dissipation (in application).
3. Maximum allowed junction temperature (125°C for the XH2576). For a safe, conservative design, a temperature approximately 15°C cooler than the maximum temperatures must be selected.
4. XH2576 package thermal resistances θ_{JA} and θ_{JC} .

Total power dissipated by the XH2576 can be estimated in [Equation 10](#):

$$P_D = (V_{IN})(I_Q) + (V_O/V_{IN})(I_{LOAD})(V_{SAT})$$

where

- I_Q (quiescent current) and V_{SAT} can be found in [Typical Characteristics](#) shown previously,
- V_{IN} is the applied minimum input voltage, V_O is the regulated output voltage, and I_{LOAD} is the load current.

The dynamic losses during turnon and turnoff are negligible if a Schottky type catch diode is used.

When no heat sink is used, the junction temperature rise can be determined by [Equation 11](#):

$$\Delta T_J = (P_D)(\theta_{JA})$$

To arrive at the actual operating junction temperature, add the junction temperature rise to the maximum ambient temperature.

$$T_J = \Delta T_J + T_A$$

If the actual operating junction temperature is greater than the selected safe operating junction temperature determined in step 3, then a heat sink is required.

When using a heat sink, the junction temperature rise can be determined by [Equation 13](#):

$$\Delta T_J = (P_D)(\theta_{JC} + \theta_{interface} + \theta_{Heat\ sink})$$

The operating junction temperature is:

$$T_J = T_A + \Delta T_J$$

As in [Equation 14](#), if the actual operating junction temperature is greater than the selected safe operating junction temperature, then a larger heat sink is required (one that has a lower thermal resistance).

11. BUCK REGULATOR

A switching regulator topology in which a higher voltage is converted to a lower voltage.

Also known as a step-down switching regulator.

BUCK-BOOST REGULATOR

A switching regulator topology in which a positive voltage is converted to a negative voltage without a transformer.

DUTY CYCLE (D) Ratio of the output switch's on-time to the oscillator period.

$$\text{for buck regulator} \quad D = \frac{t_{ON}}{T} = \frac{V_{OUT}}{V_{IN}}$$

$$\text{for buck-boost regulator} \quad D = \frac{t_{ON}}{T} = \frac{|V_O|}{|V_O| + V_{IN}}$$

CATCH DIODE OR CURRENT STEERING DIODE

The diode which provides a return path for the load current when the XH2576 switch is OFF.

EFFICIENCY (η) The proportion of input power actually delivered to the load.

$$\eta = \frac{P_{OUT}}{P_{IN}} = \frac{P_{OUT}}{P_{OUT} + P_{LOSS}}$$

CAPACITOR EQUIVALENT SERIES RESISTANCE (ESR)

The purely resistive component of a real capacitor's impedance (see Figure 35). It causes power loss resulting in capacitor heating, which directly affects the capacitor's operating lifetime. When used as a switching regulator output filter, higher ESR values result in higher output ripple voltages.



Figure 35. Simple Model of a Real Capacitor

Most standard aluminum electrolytic capacitors in the 100 μ F–1000 μ F range have 0.5 Ω to 0.1 Ω ESR. Higher-grade capacitors (low-ESR, high-frequency, or low-inductance) in the 100 μ F to 1000 μ F range generally have ESR of less than 0.15 Ω .

EQUIVALENT SERIES INDUCTANCE (ESL) The pure inductance component of a capacitor (see Figure 35).

The amount of inductance is determined to a large extent on the capacitor's construction. In a buck regulator, this unwanted inductance causes voltage spikes to appear on the output.

OUTPUT RIPPLE VOLTAGE

The AC component of the switching regulator's output voltage. It is usually dominated by the output capacitor's ESR multiplied by the inductor's ripple current (ΔI_{IND}). The peak-to-peak value of this sawtooth ripple current can be determined by reading Inductor Ripple Current.

CAPACITOR RIPPLE CURRENT

RMS value of the maximum allowable alternating current at which a capacitor can be operated continuously at a specified temperature.

STANDBY QUIESCENT CURRENT (I_{STBY})

Supply current required by the XH2576 when in the standby mode

Device Support (continued)

$\overline{\text{ON}}$ /OFF pin is driven to TTL-high voltage, thus turning the output switch OFF).

INDUCTOR RIPPLE CURRENT (ΔI_{IND})

The peak-to-peak value of the inductor current waveform, typically a sawtooth waveform when the regulator is operating in the continuous mode (vs. discontinuous mode).

CONTINUOUS/DISCONTINUOUS MODE OPERATION

Relates to the inductor current. In the continuous mode, the inductor current is always flowing and never drops to zero, vs. the discontinuous mode, where the inductor current drops to zero for a period of time in the normal switching cycle.

INDUCTOR SATURATION

The condition which exists when an inductor cannot hold any more magnetic flux.

When an inductor saturates, the inductor appears less inductive and the resistive component dominates. Inductor current is then limited only by the DC resistance of the wire and the available source current.

OPERATING VOLT MICROSECOND CONSTANT ($E \cdot T_{op}$)

The product (in Volt $\cdot\mu$ s) of the voltage applied to the inductor and the time the voltage is applied. This $E \cdot T_{op}$ constant is a measure of the energy handling capability of an inductor and is dependent upon the type of core, the core area, the number of turns, and the duty cycle.

12. ORDERING INFORMATION

Ordering Information

Part Number	Device Marking	Package Type	Body size (mm)	Temperature (°C)	MSL	Transport Media	Package Quantity
XH2576-3.3	XH2576-3.3	TO-263	15.23* 10.16	- 40 to 85	MSL3	T&R	500
XH2576-5.0	XH2576-5.0	TO-263	15.23* 10.16	- 40 to 85	MSL3	T&R	500
XH2576-12	XH2576-12	TO-263	15.23* 10.16	- 40 to 85	MSL3	T&R	500
XH2576-ADJ	XH2576-ADJ	TO-263	15.23* 10.16	- 40 to 85	MSL3	T&R	500

13. DIMENSIONAL DRAWINGS

